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EFFECT OF CASING TREATMENT
ON OVERALL AND BLADE-ELEMENT
PERFORMANCE OF A COMPRESSOR ROTOR

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EFFECT OF CASING TREATMENT ON OVERALL AND BLADE-ELEMENT PERFORMANCE OF A COMPRESSOR ROTOR

by Royce D. Moore, George Kovich, and Robert J. Blade
Lewis Research Center

SUMMARY

An axial-flow compressor rotor was tested at design speed with six different casings treatments across the rotor tip. Radial surveys of pressure, temperature, and flow angle were taken at several equivalent weight flows for each casing treatment. A solid casing, a skewed slot casing, a circumferentially grooved casing, and three different blade-angle slot casings were used across the tip of the rotor. All the casing treatments significantly decreased the weight flow at stall over that for the solid casing. A bladeangle slot configuration with slots over the middle portion of the rotor tip gave higher pressure ratio and efficiency over the entire blade span than the two blade-angle slot configurations with slots that extended past both leading and trailing edges of the blade. The rotor gave the highest overall pressure ratio with the skewed slot casing, but the efficiency was low. The rotor efficiency was the highest with the circumferentially grooved casing. The pressure ratio of the rotor was about the same for both the circumferentially grooved casing and the short blade-angle slot casing at the stall condition. However, the rotor stalled at a higher weight flow with the grooved casing than with the short blade-angle slot casing. Radial surveys indicate that the performance over the entire blade span is affected by the casing treatment applied across the tip of the rotor. The survey data showed that the losses associated with the casing treatments are higher than those for the solid casing. This would indicate that the phenomena associated with casing treatment is one of stabilizing the flow rather than one of reducing losses.

INTRODUCTION

The fan and compressor of modern aircraft must be capable of operating over widely diverse conditions. Improving the flow margin between the fan or compressor operating point and the stall-limit point will, in general, improve the useful operating range of the

propulsion system. Under many conditions, unstable flow conditions are initiated in the tip region of a fan or compressor. Thus, if stall in the tip region can be delayed, the weight flow range of the fan or compressor may be increased.

One approach to delaying stall and thus improving the weight-flow range has been to use various casing-treatment configurations across the tip of the rotor blade (refs. 1 to 3). The results of reference 1 showed that several different casing-treatment designs improved the weight-flow range (delayed stall) over that for a solid casing. The overall performance results, which were based on fixed instrumentation, showed a significant decrease in efficiency for some of the casing-treatment configurations.

The objective of this report is to present data obtained from detailed surveys of the flow conditions at the inlet and outlet of the rotor blade for some of the casing-treatment configurations of reference 1. Radial surveys of pressure, temperature, and flow angle were taken at design speed for several weight flows. For the near-stall conditions, the radial distribution of several performance parameters are compared for the various configurations. The casing-treatment configurations tested were a solid casing, three different blade angle slot configurations, a circumferentially grooved configuration, and a skewed slot configuration. This investigation was conducted at the NASA Lewis Research Center. The data are presented in tabular form as well as in plots. All symbols and equations are defined in appendixes A and B. The definitions and U.S. Customary units used in the tables are listed in appendix C, and the conversions to SI units are given in appendix D.

APPARATUS

Test Facility

A schematic view of the test facility is shown in figure 1. The facility is the same as that described in reference 1. The drive system consists of an electric motor with a variable-frequency speed control. The drive motor was coupled to a 5.02-ratio speed-increaser gear box that drove the rotor. Atmospheric air was used as the working fluid. A plenum tank 6 feet (1.83 m) in diameter and approximately 12 feet (3.66 m) long was located just upstream of the test rotor. A bellmouth nozzle was fitted from the plenum tank to the inlet of the rotor. Airflow was controlled by the butterfly valve in the outlet line.

Instrumentation

The weight flow was determined from measurements on a thin-plate orifice that was

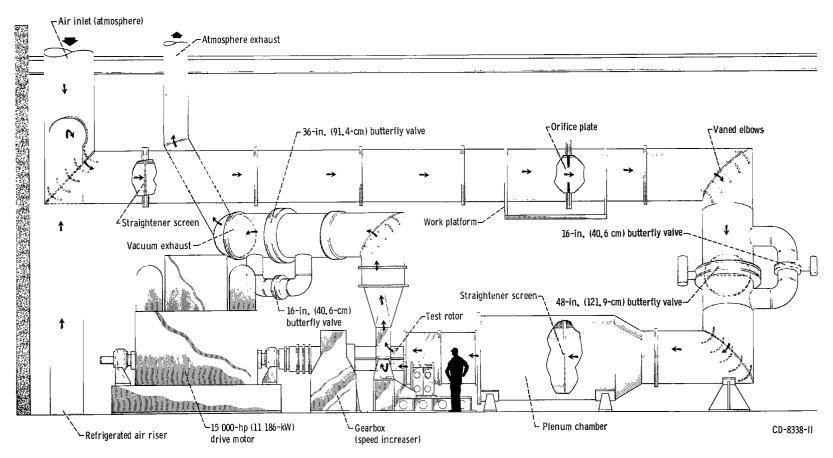


Figure 1. - Test facility.

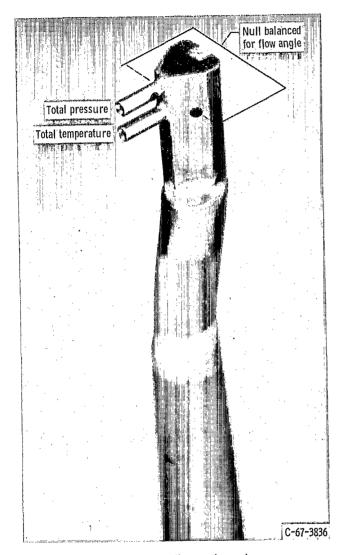


Figure 2. - Combination sensing probe.

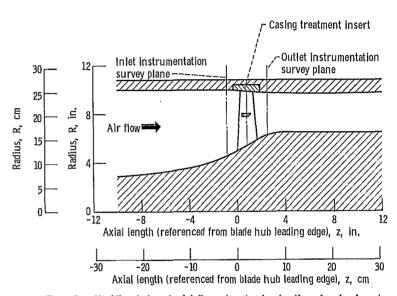


Figure 3. - Meridional view of axial-flow rotor showing location of casing insert.

27. 2 inches (69.1 cm) in diameter. The orifice plate was located in the 48-inch (121.9-cm) inlet line (fig. 1).

Radial surveys of the flow were made using combination probes (fig. 2). Four probes located approximately 90° apart were used at both the rotor inlet and outlet. The axial location of these probes is shown in figure 3. Radial distributions of total pressure and total temperature were obtained from the combination probe for both inlet and outlet conditions. The flow angles were determined from the null-balanced combination probes. The static pressure at the rotor inlet was also determined from the combination probe. However, at the rotor outlet Mach numbers were too high for accurate static-pressure measurement from the combination probe. Thus, the static pressure was assumed to vary linearily between measured outer- and inner-wall static pressures.

A hot-wire anemometer probe located approximately 1 inch (2.54 cm) upstream of the rotor leading edge was used for detecting the onset of stall. Evidence of rotor stall was also correlated by a drop in rotor outlet pressure, which was monitored on an X-Y recorder during the tests. The noise level also increased when the rotor stalled. The estimated errors of the data based on the inherent accuracies of the instrumentation and recording system are as follows:

Weight flow, lbm/sec (kg/sec)
Temperature, ${}^{O}R$ (K)
Flow angle, deg
Rotor speed, rpm
Inlet total pressure, psi (N/cm^2) ± 0.05 (± 0.03)
Inlet static pressure, psi (N/cm^2)
Outlet total pressure, psi (N/cm^2)
Outlet wall static pressure, psi (N/cm^2)

Test Rotor

The rotor used in this investigation has a nominal radius of 10 inches (25.4 cm). The 47-blade rotor has an inlet hub-tip radius ratio of 0.5. The rotor (fig. 4) was equipped with blade vibration dampers, located at about 43-percent span from the tip. The rotor (herein referred to as rotor 5) was designed for the first stage of a high-pressure-ratio axial-flow compressor. The design for this rotor is given in detail in reference 4. The design parameters for this rotor are given in tables I to III. The values listed in tables I to III are in U.S. Customary units. Conversions for SI units are given in appendix D.

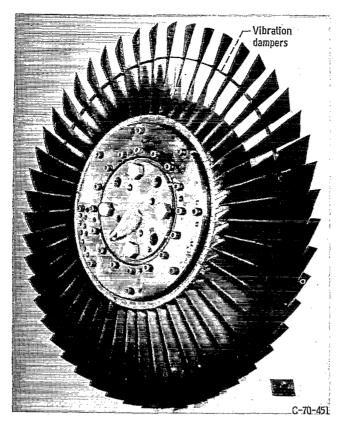


Figure 4. - Compressor rotor 5.

Casing Inserts

The casing treatments were fabricated as inserts to fit in a casing recess over the tip of the rotor blades (fig. 3). The inserts were designed to fit flush with the wall fairing. Six different casing inserts were designed. Each insert was machined so that the casing treatment surface was parallel to the rotor tip with a nominal clearance of 0.020 inch (0.05 cm). As a result of the rotor-tip taper, the inserts have about a 4° slope from the inlet to the outlet.

The casing inserts are described in detail in reference 1; thus only a brief description of each will be presented.

Solid insert. - The solid insert was used as the reference casing-treatment configuration to determine the rotor performance without casing treatment.

Blade-angle slot inserts. - Three different blade-angle slot inserts were tested. The slots, which were cut to the same angle as the blade-tip setting angle (~58°), extended radially into the casing. The radial depth and axial length of the slots varied as shown in figure 5. The insert shown in figure 5(a) will be referred to as the deep, long blade-angle slots; the insert shown in figure 5(b) will be referred to as the shallow, long

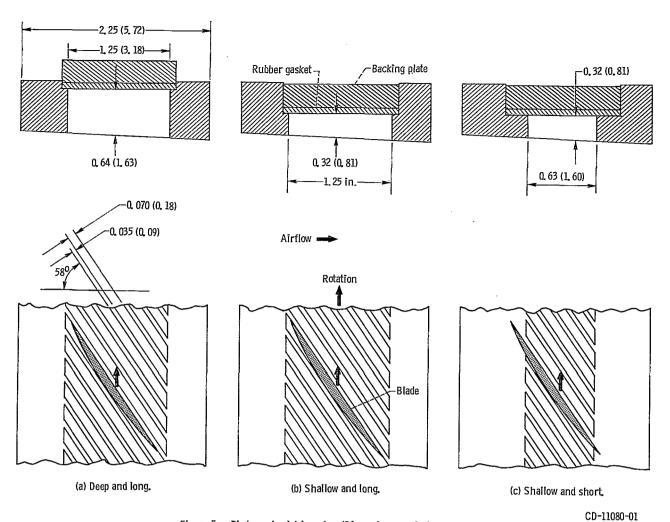
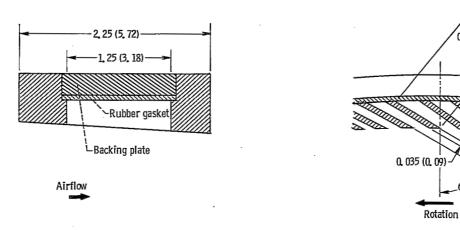


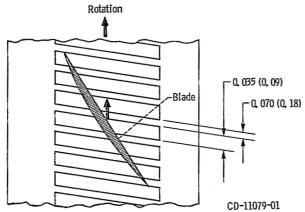
Figure 5. - Blade angle slot inserts. (Dimensions are in inches (cm).)

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Figure 6. - Shallow, short blade-angle slot insert.



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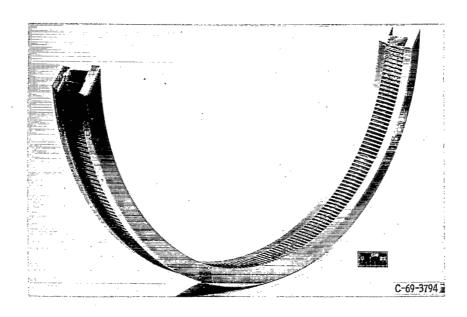
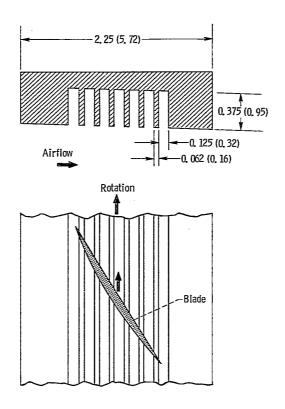


Figure 7. - Skewed slot insert. (Dimensions are in inches (cm).)



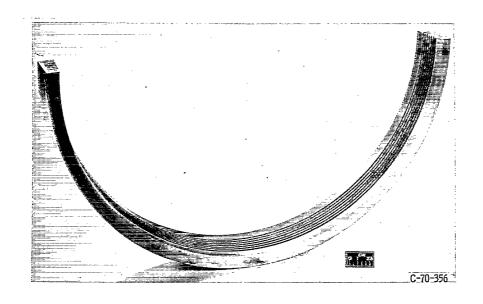


Figure 8. – Circumferentially groove insert. (Dimensions are in inches (cm),)

both the blade leading and trailing edges. The insert shown in figure 5(c) will be referred to as the shallow, short blade-angle slots. For this insert, the slots cover only the midportion of the blades. All three of these inserts have a backing plate and a rubber gasket over the back of the slots. The plate and gasket close the slots and should eliminate the slot to slot recirculation of air. However, recirculation along a slot from the trailing edge to the leading edge of the blade is possible for both of the long-slot inserts. A photograph of the shallow, short blade-angle slot insert is presented in figure 6. Wood plugs were used in the front and rear portions of the shallow, long blade-angle slot to make the shallow, short blade-angle slot.

Skewed slot insert. - The skewed slots were designed to be parallel to the axial direction and skewed in the direction of rotation. However, the slots were about 4° from the axial direction because of the changing radius of the inner diameter of the insert. A sketch of these skewed slots as well as a photograph is shown in figure 7. The slots extend past both the blade leading and trailing edges. This insert also had a plate and a gasket over the back of the slots. Recirculation along a slot from the blade trailing edge to blade leading edge is again possible, but slot to slot recirculation should be eliminated. The skewed slots have the same slot depth (fig. 7) as the deep-long blade-angle slots.

<u>Circumferentially grooved insert.</u> - The circumferentially grooved insert is shown in figure 8. The grooves extend past both the blade leading and trailing edges. The grooves were designed to give the same surface open-to-closed area ratio over the blades as the long blade-angle slots and skewed slots. The circumferential grooves should eliminate the blade-trailing-edge to blade-leading-edge recirculation, but recirculation from blade to blade along the grooves is possible.

PROCEDURE

These tests were conducted using atmospheric air as the working fluid. The inlet control valve was in the fully open position for all tests. Vacuum exhaust (26 torr vacuum) was used at the outlet of the throttle valve to help overcome system losses. The flow was controlled by manually operating the outlet throttle valve. For each casing insert, radial surveys were conducted at several weight flows for design speed only.

The overall rotor performance is based on mass-averaged values of temperature and energy-averaged values of pressure at the rotor inlet and outlet. These values were determined by the radial surveys of temperature and pressure. All parameters were based on correcting the measurements to standard day conditions at the rotor inlet. The blade-element data presented have been translated to the rotor leading and trailing edges.

The list of symbols and equations used are listed in appendixes A and B. The definitions and units for the tables is presented in appendix C.

RESULTS AND DISCUSSION

The results from this investigation will be presented in three main sections. The overall rotor performance with the various casing configurations will be presented first, followed by the radial distributions of several performance parameters for each configuration. Comparisons of parameters for various configurations are then made at the near-stall condition.

The plotted data and some additional performance parameters are also presented in tabular form. For identification, the reading numbers, which correspond to the various casing configurations, are listed in table IV. The overall performance data for each configuration are listed in table V. The blade element data for each reading are then presented in tables VI to XI. All values in the tables are in U.S. Customary units and the parameters are defined in appendix B.

Overall Performance

The overall performance for rotor 5 with the various casing configurations is presented in figure 9. Total pressure ratio, total temperature ratio, and temperature-rise efficiency are plotted as functions of equivalent weight flow for design speed. The solid data points represent the lowest flow that could be obtained just before stall. The solid line represents the rotor performance with the solid casing (no casing treatment). The dashed lines are faired through the two groups of casing-treatment data to indicate trends only. One group of treatment data seems to form a simple extension of the pressure-ratio curve for the solid-casing configuration. The second group of treatment data has about the same flow range as the first group, but the pressure ratio is considerably lower. All the casing configurations improved the weight-flow rate over that for the solid casing.

With both the deep, long and shallow, long blade-angle slot configurations, the pressure ratio and efficiency are significantly less than those values with the shallow, short blade-angle slot configuration. The efficiency with the shallow, short blade-angle slot configuration was just slightly less than that with the solid casing. The weight flow at the near-stall conditions is approximately the same for all three blade-angle slot configurations.

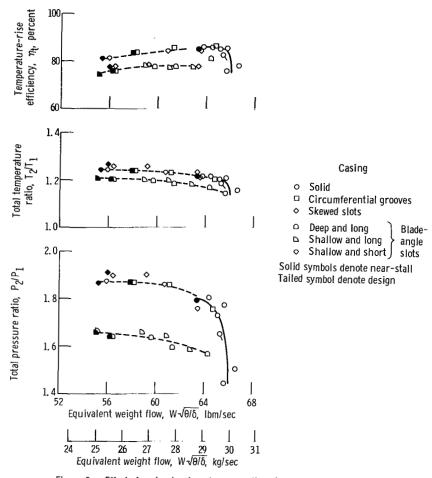


Figure 9. - Effect of casing treatment on overall performance of rotor 5. Design speed.

With the skewed slot configuration, the weight flow at the near-stall condition is about the same as it was with the three blade-angle slot configurations. At this near-stall condition, the rotor pressure ratio is the highest with the skewed slot configuration, but the efficiency with this configuration is about the same as that with both of the long blade-angle slot configurations. The skewed slot configuration has slots the same axial length as both the long blade-angle slot configurations.

The rotor operated with the circumferentially grooved configuration stalled at a slightly higher weight flow than with any of the slotted configurations. The weight flow at stall was, however, less than that for the solid casing. The maximum efficiency for this rotor with the grooved configuration is slightly greater than that obtained for the solid casing.

In general, the trends just discussed for this rotor with the various casing treatment configurations are the same as those observed in reference 1. The magnitude of weight

flow, pressure tatio, temperature ratio, and efficiency are, however, different because of the calculation procedures. Herein, the values are based on mass-averaged radial survey data corrected to standard-day conditions at the rotor inlet. In reference 1 the values were based on arithmetically averaged fixed-rake instrumentation data corrected to standard-day conditions at the plenum.

Radial Distribution

The radial distribution of several performance parameters will be examined in their relation to the trends observed in the overall performance plots. The radial distributions are presented for the various casing configurations in figures 10 to 15. The following parameters are presented as functions of percent span from the rotor tip: total pressure ratio, total temperature ratio, temperature-rise efficiency, outlet flow angle, diffusion factor, total loss coefficient, outlet tangential velocity, and outlet axial velocity. For each configuration, the parameters are presented tor three weight flows: near-stall, midflow, and near-choke conditions.

Vibration dampers were located at approximately 43-percent span from the rotor tip. Data points were more closely spaced in the damper region in order to define the damper wake and to get more accurate mass-averaged values.

Solid casing. - The radial distributions for this rotor with the solid casing are presented in figure 10. The design distributions are also shown in this figure as dashed

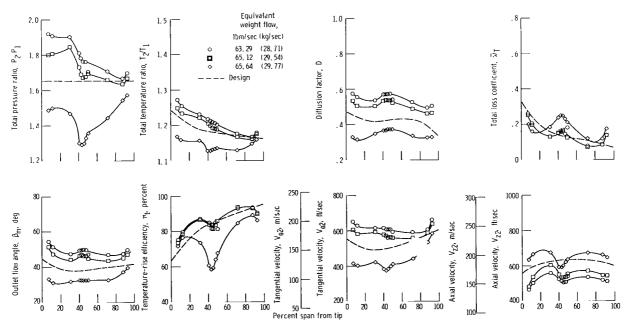


Figure 10. - Radial distribution of performance for rotor 5 operated with solid casing. Design speed.

lines. As the flow was decreased, the pressure ratio increased, particularly in the tip region. The diffusion factor and tangential velocity also increased fairly uniformly across the entire blade span. Except near the tip, the losses decrease with decreasing weight flow. Examination of the outlet axial velocity indicates that as the throttle valve was closed the flow decreased uniformly across the blade span.

The total pressure ratio shows a decay in the region of the dampers (~43 percent span). Except at the highest weight flow, the total temperature ratio did not show the decay in the damper region. The loss in efficiency is due to the loss in total pressure. Although the diffusion factor at the near-stall condition is higher than the design value, the losses are less than the design values except in the damper and hub regions.

Deep, long blade-angle slot casing. - The radial distributions for the deep, long blade-angle slot casing configurations are presented in figure 11. For all three weight flows, the total pressure shows a sharp decrease from about 30-percent span to the tip. The differences in efficiency for the three weight flows from the tip to about 30-percent span is attributed to the change in total temperature ratio. The flow in the tip region is low, as evidenced by the low axial velocity at the rotor outlet. The losses in the tip region increased rapidly with decreasing weight flow. At the near-stall condition, the blade shows an increase in loading (diffusion factor) from 30-percent span to the tip; at the other two weight flows, the loading decreases.

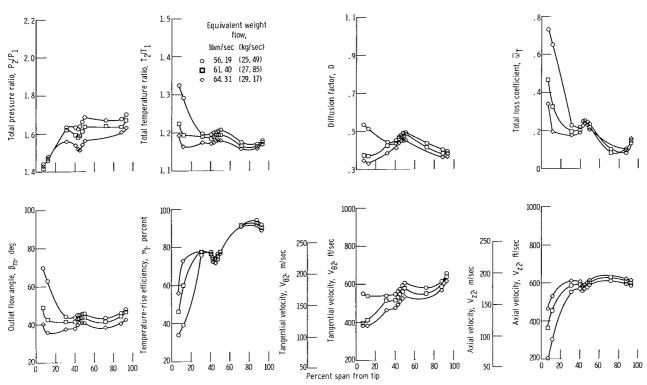


Figure 11. - Radial distribution of performance for rotor 5 operated with deep, long blade-angle slot casing. Design speed.

It is evident that the effect of this casing treatment is felt over the entire blade span when comparisons are made with the solid casing configuration. At a comparable weight flow with the solid casing, the pressure ratio over the entire blade span is much lower, and the losses are much higher with the deep, long blade-angle slot configuration. This is probably due to considerable recirculation at the rotor tip, which causes the stream-lines to shift over the entire blade span.

Shallow, long blade-angle slot casing. - The radial distributions for the shallow, long blade-angle slot casing configuration are presented in figure 12. The rotor in this

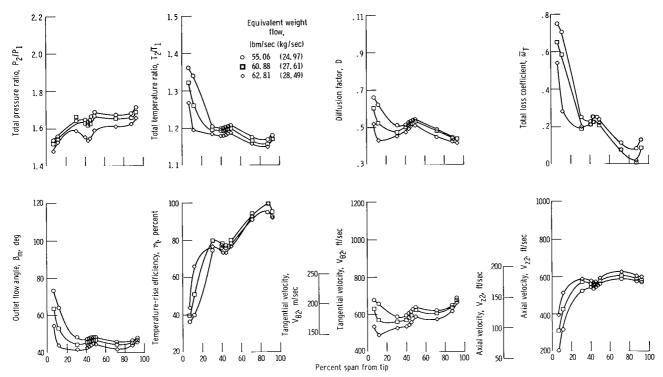


Figure 12. - Radial distribution of performance for rotor 5 operated with shallow, long blade-angle slot casing. Design speed.

configuration gave similar trends as it did with the deep, long blade-angle slot configuration. However, the diffusion factor for the two higher weight flows increased from 30-percent span to the tip. The losses in the tip region are high for all three weight flows. The axial velocity at the rotor outlet is low in the tip region, indicating a reduction in flow in this region.

Shallow, short blade-angle slot casing. - The radial distributions for the shallow, short blade-angle slot casing configuration are given in figure 13. At each radial location, the pressure ratio, temperature ratio, outlet flow angle, diffusion factor, outlet tangential velocity, and total loss coefficient increased with decreasing weight flow.

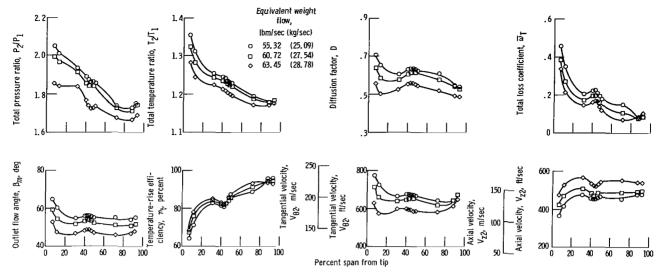


Figure 13. - Radial distribution of performance for rotor 5 operated with shallow, short blade-angle slot casing. Design speed,

For the highest weight flow, the pressure ratio remained essentially constant from 30-percent span to the tip. However, at the two other weight flows, the pressure ratio continued to increase to the tip. Except in the hub region, the efficiency over the blade span decreased as the weight flow decreased. With this configuration, the large decrease in axial velocity in the tip region experienced with the two long blade-angle slot configurations was not observed. There was a slight decrease in axial velocity in the tip region.

The rotor with the solid casing stalled at a weight flow of about 63.3 pounds per second (28.71 kg/sec). At a comparable weight flow of 63.45 pounds per second (28.78 kg/sec), the rotor with the shallow, short blade-angle slot casing has about the same radial distribution of parameters as it did with the solid casing. The absolute values are approximately the same for both casing configurations. The losses in the tip region are slightly greater for the shallow, short blade-angle casing. The shallow, short blade-angle slot casing configuration allowed the blade loading (diffusion factor) to continue to increase while the weight flow was decreased to values less than the stall weight flow for the solid casing. The flow decreased about 8 pounds per second (3.6 kg/sec) below that value for the solid casing configuration before stall occurred.

Skewed slot casing. - The radial distribution for the skewed slot casing configuration is presented in figure 14. Both the total temperature and total pressure show a decrease from 12-percent span to 7-percent span. The pressure ratio in the tip region remained essentially constant as the weight flow was reduced from 59. 20 to 55. 99 pounds per second (26. 85 to 25. 40 kg/sec). With this configuration, the midpassage of the blade is more highly loaded (higher diffusion factor) than the tip for all three weight flows.

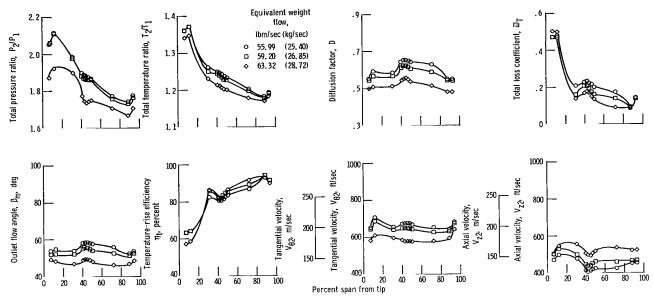


Figure 14. - Radial distribution of performance for rotor 5 operated with skewed slot casing. Design speed.

At the weight flow at which the solid casing configuration stalled (63.29 lbm/sec (28.71 kg/sec)), this casing treatment configuration showed about the same trends in radial distribution as the solid casing, except in the tip region. The apparent losses in the tip region are much greater for the skewed slot configuration although the diffusion factor is about the same for both the solid and skewed slot configurations. For this slot configuration, the momentum-rise efficiency is about 8 to 10 percentage points greater than the temperature-rise efficiency (table V(e)). This would indicate that there is considerable recirculation in the tip region. Perhaps if the slots were confined to only the midportion of the blade tips as they were for the shallow, short blade angle slot configuration, the recirculation would have been reduced. Then, the efficiency curve might have been an extension of the solid casing efficiency curve just as the pressure ratio curve seemed to be an extension of the solid casing pressure ratio curve in the overall performance maps of figure 9.

Circumferentially grooved casing. - The radial distributions for the circumferentially grooved casing configuration are presented in figure 15. The total pressure ratio increased from 30-percent span to the tip for the two lower weight flows but remained essentially constant for the highest weight flow. Except in the hub region, the efficiency along the blade span decreased with decreasing weight flow.

At a comparable weight flow, the radial distributions were about the same for the grooved configuration as the solid casing configuration. The losses, however, were just slightly greater in the tip region for the grooved configuration. With the circumferentially grooved casing configuration, the rotor could continue to load up (increase

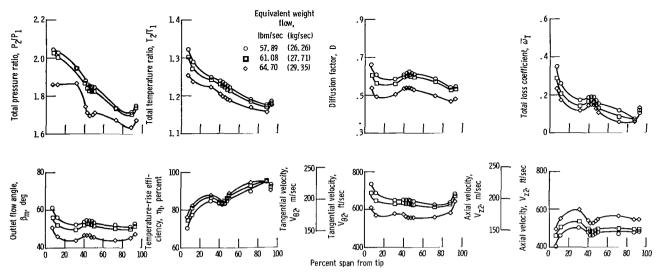


Figure 15. - Radial distribution of performance for rotor 5 operated with circumferential groove casing. Design speed.

diffusion factor) as the weight flow was reduced to a value less than the stall weight flow with the solid casing. This accounts for the overall pressure ratio and efficiency curve for the grooved configuration being a continuation of the curves for the solid casing configuration.

CASING TREATMENT COMPARISONS

One objective of the casing treatment was to decrease the weight flow at which stall occurs as compared with a solid casing, thereby increasing the useful operating range of the rotor. Thus, comparisons of the various casing configurations are made at the near-stall condition. The various performance parameters are again presented as a function of percent span.

In figure 16, the rotor performance with the three different blade-angle slot configurations are compared. With both long slot configurations, all the plotted parameters exhibit the same trends with percent span. The efficiency and losses are essentially the same for the two configurations. For the shallow, short blade-angle slot configuration, the pressure ratio and temperature ratio continually decreased with increasing percent span except near the hub. For both long blade-angle slot configurations, the pressure ratio increased from the tip to midspan and then remained relatively constant to the hub. The short slot configuration gave higher pressure ratio and efficiency over the entire blade span than did the two long slot configurations. The blade loading with the short slot configuration was uniformly higher across the entire span than with either of the long slot configurations. With the long slot configurations, the rotor with shallow slots

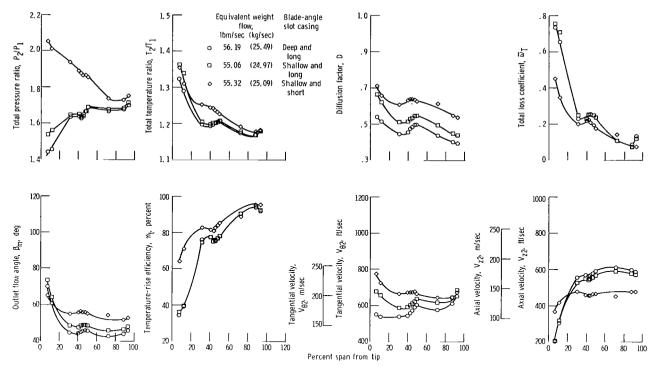


Figure 16. - Comparison of radial distribution of performance for rotor 5 for the three different blade-angle slot casings. Design speed; near-stall conditions,

was more highly loaded than it was with deep slots. Examination of all the parameters presented show that the performance of this rotor is appreciably improved with the shallow, short blade-angle slot configuration over that for either the deep, long or shallow, long blade-angle slot configurations.

In figure 17, the parameters at the near-stall condition are compared for the shallow, short blade-angle slot, skewed slot, and circumferentially grooved configurations. The radial distributions are similar with the three different configurations except in the tip region with the skewed slot configuration. The pressure ratio of the rotor with the grooved configuration is almost identical to that with the shallow, short blade-angle slot configuration, even though the weight flow is different. The temperature ratio is less with the grooved configuration thereby giving a higher efficiency than with the blade-angle slot configuration. The pressure ratio and temperature ratio are the highest with the skewed slot configuration except in the tip region. At 7-percent span, the pressure ratio is about the same as that for the shorter blade-angle slot and grooved configurations. The efficiency, however, is the lowest with the skewed slot configuration. Both pressure ratio and temperature ratio showed a decrease from 12-percent span to the tip with the skewed slot configuration.

At the near-stall condition, the rotor blades with the shallow, short blade-angle slot configuration are more highly loaded over the entire blade span than with the grooved configuration. This is due at least in part to the lower weight flow at which the rotor

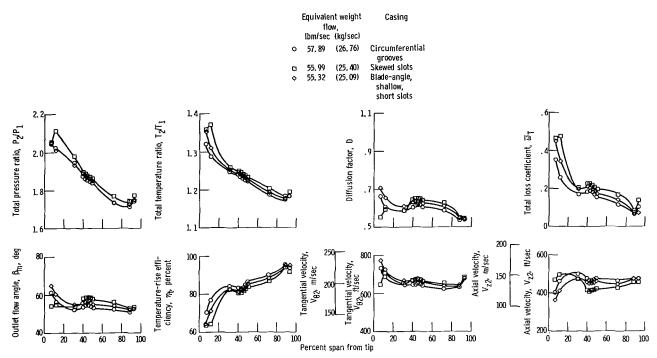


Figure 17. - Comparison of radial distribution of performance for rotor 5 for several different casings. Design speed; near-stall conditions.

stalled with the blade angle slot configuration. With the skewed slot configuration, the blade loading was lower in the tip region and higher from midspan to the hub region than either the blade-angle slot or grooved configuration. The losses at the near-stall condition are the lowest with the grooved configuration and highest with the skewed slot configuration.

Shortening the slots in the blade-angle slot configuration improved the pressure ratio in the tip region (fig. 16). The pressure ratio in the tip region with the skewed slot configuration might not show the decrease from 12-percent span to the tip had the slots been shorter.

CONCLUDING REMARKS

The results from this investigation indicate that the casing-treatment slots probably should not extend past the blade leading and trailing edges if both high efficiency and pressure ratio are to be achieved. The shorter blade-angle slot configuration gave higher efficiency and pressure ratio than both blade-angle slot configurations with slots that extended past the blade edges. The skewed slot configuration, which also had slots extending past the blade edges, had high pressure ratio, but the efficiency was low because of recirculation.

The overall performances for the shallow, short blade-angle slot and for the circumferentially grooved casing configurations fall close to an extension of the overall performance for the solid casing (fig. 9). However, the survey data indicate that the losses associated with the casing treatments are higher than those for the solid casing at comparable weight flow. This would indicate that the phenomena associated with casing treatment is one of flow stabilization rather than one of loss reduction. The stabilization of the flow delays stall, thereby allowing the weight flow to be reduced over that of the solid casing. More detailed measurements near the tip leading and trailing edges and dynamic measurements over the rotor tips may be necessary in order to further define the phenomena.

SUMMARY OF RESULTS

An axial-flow compressor rotor was tested at design speed with six different casing-treatment configurations. A solid, three different blade-angle slots, a skewed slot, and a circumferentially grooved casing treatment configurations were used. Radial surveys of the flow conditions (pressure, temperature, and flow angle) into and out of the rotor were taken at several weight flows for each configuration. This investigation yielded the following principal results:

- 1. The weight flow at which the rotor stalled decreased significantly with all the casing-treatment configurations below that with the solid casing.
- 2. A blade-angle slot configuration with slots over the middle portion of the rotor blade tips gave higher pressure ratio and efficiency over the entire blade span than two blade-angle slot configurations with slots that extended beyond both blade leading and trailing edges. Radial surveys indicated that the losses were lower for the shorter blade angle slot configuration.
- 3. At the near-stall condition, the total pressure ratio of the rotor with the skewed slot configuration was higher than with any other configuration from 7-percent span to the hub. At 7-percent span from the tip, the pressure ratio was about the same as that for the shorter blade-angle slot and circumferentially grooved configurations. However, the efficiency was lower than that with the shorter blade-angle slot and circumferentially grooved configuration.
- 4. The rotor with the circumferentially grooved configuration had the highest efficiency; and its pressure ratio was about the same as with the shorter blade angle slot

configurations. However, the rotor stalled at a higher weight flow with the grooved configuration than with the blade-angle slot or skewed-slot configurations.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, August 3, 1971,
720-03.

APPENDIX A

SYMBOLS

```
annulus area at rotor leading edge. 1.59 ft<sup>2</sup> (0.0148 m<sup>2</sup>)
A<sub>an</sub>
        frontal area at rotor leading edge, 2.13 ft<sup>2</sup> (0.0198 m<sup>2</sup>)
A_{f}
        specific heat at constant pressure, 0.24 Btu/(lb)(OR) (1004 J/(kg)(K))
C_{\mathfrak{p}}
        diffusion factor
D
        acceleration of gravity, 32, 17 ft/sec<sup>2</sup> (9, 8 m/sec<sup>2</sup>)
g
^{i}mc
        mean incidence angle, angle between inlet air direction and line tangent to blade
           mean camber line at leading edge, deg
        suction surface incidence angle, angle between inlet-air direction and line tangent
i<sub>ss</sub>
           to blade suction surface at leading edge, deg
J
        mechanical equivalent of heat, 778. 16 ft-lb/Btu
N
        rotative speed, rpm
        total pressure, psia (N/cm<sup>2</sup>)
\mathbf{p}
        static pressure, psia (N/cm<sup>2</sup>)
р
        radius, in. (cm)
\mathbf{r}
        total temperature, <sup>O</sup>R (K)
Т
U
        wheel speed, ft/sec (m/sec)
V
        air velocity, ft/sec (m/sec)
W
        weight flow, lbm/sec (kg/sec)
        axial distance referenced from rotor blade hub leading edge, in. (cm)
\mathbf{z}
        air angle, angle between air velocity and axial direction, deg
β
        ratio of specific heats (1.40)
γ
        ratio of rotor inlet total pressure to standard pressure of 14.69 psia
δ
           (10.13 \text{ N/cm}^2)
\delta^{O}
        deviation angle, angle between exit air direction and tangent to blade mean cham-
           ber line at trailing edge, deg
θ
        ratio of rotor inlet total temperature to standard temperature of 518.7° R
           (288.1 K)
        efficiency
η
```

 κ_{mc} angle between the blade mean camber line and the axial direction, deg

 $\kappa_{_{\mbox{\footnotesize{\bf SS}}}}$ angle between the blade suction surface camber line at the leading edge and the axial direction, deg

σ solidity, ratio of chord to spacing, c/s

 $\overline{\omega}$ total loss coefficient

 $\overline{\omega}_{\rm p}$ profile loss coefficient

 $\omega_{\rm s}$ shock loss coefficient

Subscripts:

id ideal

LE blade leading edge

m meridional direction

mom momentum

TE blade trailing edge

t temperature-rise (adiabatic)

 θ tangential direction

1 instrument plane upstream of rotor

2 instrument plane downstream of rotor

Superscripts:

relative to rotor

APPENDIX B

PERFORMANCE PARAMETERS

Suction surface incidence angle:

$$i_{SS} = \left(\beta_{m}^{\prime}\right)_{LE} - (\kappa_{SS}) \tag{B1}$$

Mean incidence angle:

$$i_{mc} = \left(\beta'_{m}\right)_{LE} - \left(\kappa_{mc}\right)_{LE} \tag{B2}$$

Deviation:

$$\delta^{O} = \left(\beta_{\mathbf{m}}^{\dagger}\right)_{\mathbf{TE}} - \left(\kappa_{\mathbf{mc}}\right)_{\mathbf{TE}} \tag{B3}$$

Diffusion factor:

$$D = 1 - \frac{(V')_{TE}}{(V')_{LE}} + \frac{(rV_{\theta})_{TE} - (rV_{\theta})_{LE}}{(r)_{LE} + (r)_{TE}]\sigma(V')_{LE}}$$
(B4)

Total loss coefficient:

$$\overline{\omega} = \frac{\left(P'_{id}\right)_{TE} - \left(P'\right)_{TE}}{\left(P'\right)_{LE} - \left(p\right)_{LE}}$$
(B5)

Profile loss coefficient:

$$\overline{\omega}_{p} = \overline{\omega} - \overline{\omega}_{s}$$
 (B6)

Total loss parameter:

$$\frac{\overline{\omega} \cos\left(\beta'_{\text{mc}}\right)_{\text{TE}}}{2\sigma} \tag{B7}$$

Profile loss parameter:

$$\frac{(\overline{\omega} - \overline{\omega}_{s})\cos(\beta_{mc}^{\dagger})_{TE}}{2\sigma}$$
 (B8)

Temperature-rise efficiency:

$$\eta_{t} = \frac{\frac{(P)_{TE}}{(P)_{LE}} - 1}{\frac{(T)_{TE}}{(T)_{LE}} - 1}$$
(B9)

Momentum rise efficiency:

$$\eta_{\text{mom}} = \frac{\left[\frac{(P)_{\text{TE}}}{(P)_{\text{LE}}}\right]^{(\gamma-1)/\gamma} - 1}{\frac{(UV\sigma)_{\text{TE}} - (UV\sigma)_{\text{LE}}}{(T)_{\text{LE}}gJC_{p}}}$$
(B10)

Equivalent weight flow:

$$\frac{\mathbf{W}\sqrt{\theta}}{\delta} \tag{B11}$$

Equivalent rotative speed:

$$\frac{N}{\sqrt{\theta}}$$
 (B12)

Weight flow per unit frontal area:

$$\frac{\mathbf{W}\sqrt{\theta}}{\delta}$$

$$\mathbf{A_f}$$
(B13)

Weight flow per unit annulus area:

$$\frac{\mathbf{W}\sqrt{\theta}}{\delta}$$
A_{an} (B14)

Head rise coefficient:

$$\frac{\text{gJC}_{\text{p}}\text{T}_{\text{LE}}}{(\text{U}_{\text{tip}})^2} \left[\left(\frac{\text{P}_{\text{TE}}}{\text{P}_{\text{LE}}} \right) \right]^{(\gamma-1)/\gamma} - 1$$
(B15)

Flow coefficient:

$$\left(\frac{\mathbf{V}_{\mathbf{Z}}}{\mathbf{U}_{\mathbf{tip}}}\right)_{\mathbf{LE}}$$
 (B16)

APPENDIX C

DFFINITIONS AND UNITS USED IN TABLES

ABS absolute

AREA RATIO ratio of actual flow area to critical area (where local Mach number

is one)

BETAM meridional air angle, deg

CONE ANGLE angle between axial direction and conical surface representing blade

element, deg

DELTA INC difference between mean camber blade angle and suction surface blade

angle, deg

DEV deviation angle (defined by eq. (B3)), deg

D-FACT diffusion factor (defined by eq. (B4))

EFF temperature-rise efficiency (defined by eq. (B9))

IN inlet (leading edge of blade)

INCIDENCE incidence angle (suction surface defined by eq. (B1) and mean defined

by eq. (B2))

KIC angle between blade mean camber line and axial direction at leading

edge, deg

KOC angle between blade mean camber line and axial direction at trailing

edge, deg

KTC angle between blade mean camber line and axial direction at transition

point, deg

LOSS COEFF loss coefficient (total defined by eq. (B5) and profile defined by

eq. (B6))

LOSS PARAM loss parameter (total defined by eq. (B7) and profile defined by

eq. (B8))

MERID meridional

MERID VEL R meridional velocity ratio

OUT outlet (trailing edge of blade)

PHISS suction surface camber ahead of assumed shock location, deg

PRESS pressure, psia

PROF profile

RADII radius, in.

REL relative to the blade

RI inlet radius (leading edge of blade), in.

RO outlet radius (trailing edge of blade), in.

RP radial position

RPM rotative speed, rpm

SPEED speed, ft/sec

SS suction surface

STREAMLINE SLOPE slope of streamline, deg

TANG tangential

TEMP temperature, ^OR

TI thickness of blade at leading edge, in.

TM thickness of blade at maximum thickness, in.

TO thickness of blade at trailing edge, in.

TOT total

VEL velocity, ft/sec

X FACTOR ratio of suction surface camber ahead of assumed shock loca-

tion of multiple circular arc blade section to that of double

circular arc blade section

ZMC axial distance to blade maximum thickness point from inlet, in.

ZOC axial distance to blade trailing edge from inlet, in.

ZTC axial distance to transition point from inlet, in.

APPENDIX D

CONVERSION FACTORS FOR SI UNITS

Length:

1 inch = 2.54 centimeter

1 foot = 0.3048 meter

Temperature:

 $1^{O} R = 0.55555 K$

Pressure:

1 psia = $0.68947572 \text{ N/cm}^2$

Velocity and speed:

1 ft/sec = 0.3048 m/sec

Weight flow:

1 lbm/sec = 0.45359237 kg/sec

Weight flow per area: $1 \text{ lbm/sec ft}^2 = 0.042140 \text{ kg/sec m}^2$

REFERENCES

- 1. Osborn, Walter M.; Lewis, George W.; and Heidelberg, Laurence J.: Effect of Several Porous Casing Treatments on Stall Limit and Overall Performance of an Axial-Flow Compressor Rotor. NASA TN D-6537, 1971.
- 2. Bailey, Everett E.; and Voit, Charles H.: Some Observations of Effects of Porous Casings on Operating Range of a Single Axial-Flow Compressor Rotor. NASA TM X-2120, 1970.
- 3. Koch, C. C.: Experimental Evaluation of Outer Case Blowing or Bleeding of Single-Stage Axial-Flow Compressor, Part VI. Rep. R69AEG256, General Electric Co. (NASA CR-54592), Jan. 30, 1970.
- 4. Ball, Calvin L.; Janetske, David C.; and Reid, Lonnie: Performance of a 1380-Foot-Per-Second-Tip-Speed Axial-Flow Compressor Rotor with Blade Tip Solidity of 1.5. NASA TM X-2379, 1971.

TABLE I. - DESIGN OVERALL PARAMETERS FOR ROTOR 5

TOTAL PRESSURE RATIO	1.652
TOTAL TEMPERATURE RATIO	1.187
EFFICIENCY	0.824
HT FLOW PER UNIT FRONTAL AREA	30.824
HT FLOW PER UNIT ANNULUS AREA	41.549
HT FLOH	65.284
RPM 160	000.000
TIP SPEED	575.738

TABLE II. - DESIGN BLADE-ELEMENT PARAMETERS FOR ROTOR 5

RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	RP T I P 1 2 3 4 5 6 7 8 9 10 1 HUB
PERCENT SPAN 0. 7.00 11.70 30.90 40.40 45.20 47.90 50.00 71.80 93.10 100.00	ABS M 0.608 0.614 0.622 0.649 0.650 0.651 0.652 0.6589 0.589 0.568	ABS IN 654.5 661.3 667.0 689.1 695.8 696.9 697.3 698.4 681.8 635.8 615.0 589.1	RAD IN 9.853 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377 5.006
INC 1 MEAN 2.0 2.6 3.8 4.3 4.5 4.7 4.9 6.7 6.8	ACH NO OUT 0.660 0.665 0.670 0.693 0.696 0.704 0.739 0.775 0.787	VEL OUT 787.6 788.6 796.1 803.3 805.9 808.6 811.7 814.3 848.1 882.7 894.0 913.6	9.802 9.531 9.549 8.637 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201 5.934
DENCE SS 0.0 0.0 0.0 0.0 0.0 0.0 0.0	REL M IN 1.414 1.391 1.372 1.289 1.244 1.235 1.221 1.207 1.196 1.069 0.942 0.897 0.843	RELL IN 1523.5 1497.4 1475.5 1382.9 1334.0 1321.3 1308.1 1293.7 1282.1 1147.6 970.5 914.1	ABS IN -0. -0. 0. 0. 0. 0. 0.
DEV 6.0 5.1 4.6 3.7 3.8 3.9 4.9 6.1 6.8 7.7	ACH NO OUT 0.828 0.835 0.837 0.815 0.768 0.758 0.751 0.684 0.647 0.639	VEL 0UT 988.2 989.7 987.9 948.6 911.7 900.7 889.5 868.5 784.8 726.4 718.4	8 BETAM 0UT 44.7 42.3 41.0 38.0 38.1 38.5 38.5 39.8 40.9 41.3 41.6
D-FACT 0.472 0.454 0.442 0.418 0.425 0.425 0.427 0.429 0.427 0.429 0.370 0.335	MERID M 0.608 0.614 0.622 0.649 0.650 0.651 0.6552 0.6589 0.568	MERI IN 654.5 661.3 667.0 689.1 695.8 696.9 697.3 698.4 681.8 635.8 615.0 589.1	REL 1N 64.6 63.8 63.1 60.1 58.2 57.8 57.3 57.3 57.5 51.3
0.634 0.680	ACH NO 9 0.469 0.492 0.539 0.546 0.547 0.548 0.551 0.568 0.568 0.591 0.604	D YEL OUT 559.7 583.0 627.3 633.2 633.9 634.5 635.6 636.6 651.4 666.8 671.8 683.2	BETAM 0UT 55.5 53.9 52.9 48.6 46.0 45.3 44.5 43.6 42.9 33.9 25.2 22.3 18.0
LOSS C TOT 0.328 0.248 0.158 0.135 0.135 0.132 0.128 0.128 0.101 0.084 0.078 0.065	STREAML II -4.00 -3.40 -2.87 0.50 2.78 3.42 4.08 4.85 5.48 13.70 22.91 26.32 30.90	TAN IN -00. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	TOTA IN 518.7 518.7 518.7 518.7 518.7 518.7 518.7 518.7 518.7
OEFF PROF 0.221 0.173 0.145 0.072 0.066 0.068 0.069 0.073 0.073 0.081 0.077	NE SLOPE OUT -4.80 -3.53 -2.60 1.65 4.05 4.05 4.69 5.35 6.11 6.71 14.03 21.48 24.11 28.40	OUT 554.1 5531.0 490.2 494.4 497.5 501.4 9 507.8 543.2 578.4 589.7 606.5	RAT10 1.243 1.227 1.217 1.182 1.182 1.181 1.180 1.171 1.166 1.164
LOSS P TOT 0.062 0.054 0.031 0.026 0.026 0.025 0.025 0.015 0.015		IN	TOTAL IN 14.69 14.69 14.69 14.69 14.69 14.69 14.69 14.69 14.69
ARAM PROF 0.042 0.033 0.028 0.014 0.013 0.013 0.014 0.014 0.014 0.014	PEAK SS MACH NO 1.612 1.619 1.622 1.562 1.554 1.554 1.538 1.538 1.453 1.272 1.211	1305.4 1201.8 1150.4 1137.4 1124.6 1109.9	1.652 1.652 1.652 1.652 1.652 1.652

TABLE III. - BLADE GEOMETRY FOR ROTOR 5

TABLE IV. - IDENTIFICATION OF READING NUMBERS

RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	PERCENT SPAN 0. 7. 12. 31. 40. 43. 45. 48. 50. 72. 88. 93. 100.	RAD RI 9.853 9.622 9.426 8.587 8.152 8.040 7.927 7.800 6.611 5.681 5.377 5.006	R0 9.802 9.531 9.534 9.534 9.607 8.239 8.146 7.949 7.868 7.025 6.387 6.387 6.2934	BLA KIC 62.55 61.46 60.53 56.30 54.24 53.70 53.17 52.11 47.47 44.59 43.93 43.25	DE ANGL KTC 58.39 56.87 55.62 50.60 48.35 47.70 46.25 45.64 38.40 31.77 29.63 27.05	ES KOC 49.50 48.77 48.18 45.02 42.31 41.52 40.58 39.70 38.92 28.98 18.71 15.18	DELTA INC 1.95 2.29 2.57 3.81 4.30 4.42 4.55 4.69 4.80 5.88 6.55 6.68
RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	BLADE TI 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020	THICKN TM 0.060 0.064 0.085 0.095 0.095 0.097 0.101 0.123 0.140 0.153	ESSES TO 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020	AXIA ZMC 0.554 0.558 0.560 0.575 0.604 0.611 0.619 0.626 0.632 0.694 0.754 0.771	DIMEN ZTC 0.554 0.558 0.560 0.560 0.604 0.611 0.619 0.632 0.632 0.740 0.754	SIONS ZOC 1.001 1.056 1.092 1.230 1.288 1.303 1.359 1.356 1.488 1.595 1.627	CONE ANGLE -5.700 -4.831 -3.964 0.902 3.857 4.653 5.470 6.377 7.081 15.350 23.606 26.582 30.300
RP TIP 12345678910111	AERO CHORD 1,903 1,903 1,936 1,961 1,961 1,962 1,962 1,988 2,070 2,117 2,165	SETTING ANGLE 57.84 56.44 55.31 50.61 48.30 47.64 46.96 46.96 45.56 38.29 31.70 29.58 26.80		SOLIDITY 1.500 1.530 1.561 1.703 1.788 1.812 1.836 1.864 1.888 2.196 2.584 2.753 2.980	X FACTOR 0.649 0.735 0.802 1.000 1.000 1.000 1.000 1.000 1.000 1.000	PHISS 5.82 6.71 7.35 9.14 9.07 9.12 9.26 9.76 10.05 10.04	AREA RAT10 1.085 1.081 1.077 1.062 1.050 1.048 1.045 1.035 1.035 1.043

Casing	Reading numbers
Solid	443- 684
	444- 695
	445- 706
	477- 830
	478- 847
	479- 858
	482- 869
Deep, long blade-	551-1061
angle slot	552-1073
	553-1084
	554-1095
	555-1106
Shallow, long blade-	707-1503
angle slot	708-1514
	709-1525
	710-1536
	711-1547
hallow, short blade-	761-1629
ngle slot	762-1640
	763-1651
	764-1662
kewed slot	508- 924
	510- 940
	511- 951
	512- 962
ircumferentially	602-1227
rooved	603-1238
	604-1249
	605-1260

TABLE V. - OVERALL PERFORMANCE FOR ROTOR 5 WITH DIFFERENT ROTOR CASINGS

(a) With solid casing

		Reading number						
·	443-684	444-695	445-706	477-830	478-847	479-858	482-869	
ROTOR TOTAL PRESSURE RATIO	1.805	1.505	1,776	1.792	1.447	1.731	1.79	
ROTOR TOTAL TEMPERATURE RATIO	1.214	1.158	1.209	1.213	1,147	1.200	1.213	
ROTOR TEMP. RISE EFFICIENCY	0.860	0.782	0.855	0.851	0.760	0.851	0.857	
ROTOR MOMENTUM RISE EFFICIENCY	0.857	0.772	0.858	0.841	0.746	0.836	0.848	
ROTOR HEAD RISE COEFFICIENT	0.300	0.202	0.290	0.299	0.183	0.279	0.299	
FLON COEFFICIENT	0.431	0.441	0.431	0.429	0.451	0.445	0.429	
MT FLOW PER UNIT FRONTAL AREA	30.405	31.452	31.032	29.883	30.992	30.745	30.062	
NT FLON PER UNIT ANNULUS AREA	40.983	42.395	41.829	40.280	41.775	41.442	40.521	
HT FLOH AT ORIFICE	64.397	66.616	65.725	63.293	65.642	65.117	63.671	
HT FLOW AT ROTOR INLET	64.897	66.054	65.000	64.491	66.783	66,141	64.553	
HT FLOH AT ROTOR OUTLET	61.023	64.188	62,441	60.458	64.000	62,382	60.554	
RPM	16083.417	16083.709	16099.760	15998.963	16009.100	16027.687	16022.704	
PERCENT OF DESIGN SPEED	100.521	100.523	100.623	99.994	100.057	100.173	100.142	

(b) With deep, long blade-angle slot casing

51-1061 	552-1073 1.568 1.169	553-1084	554-1095 1.635	555-1106
1.200		1.595	1 636	i
0.756 0.791 0.248 0.352 26.530 35.761 56.192 55.714 53.974	0.812 0.824 0.225 0.428 30.364 40.929 64.312 64.314 62.688 16042.574	1.184 0.777 0.807 0.234 0.395 28.989 39.075 61.399 60.399 59.197 16049.264	1.195 0.774 0.808 0.246 0.376 28.159 37.956 59.640 58.604 57.141	1.640 1.201 0.756 0.789 0.248 0.349 26.629 35.894 56.400 55.368 53.959
	26.530 35.761 56.192 55.714 53.974	26.530 30.364 35.761 40.929 56.192 64.312 55.714 64.314 53.974 62.688 043.216 16042.574	26.530 30.364 28.989 35.761 40.929 39.075 56.192 64.312 61.399 55.714 64.314 60.930 53.974 62.688 59.197 043.216 16042.574 16049.264	26.530 30.364 28.989 28.159 35.761 40.929 39.075 37.956 56.192 64.312 61.399 59.640 55.714 64.314 60.930 58.604 53.974 62.688 59.197 57.141 043.216 16042.574 16049.264 16061.969

(c) With shallow, long blade-angle slot casing

	Reading number					
	707-1503	708-1514	709-1525	710-1536	711-1547	
ROTOR TOTAL PRESSURE RATIO	1.657	1.585	1.642	1.659	1.665	
ROTOR TOTAL TEMPERATURE RATIO	1.209	1.181	1.197	1.199	1.208	
ROTOR TEMP. RISE EFFICIENCY	0.744	0.777	0.771	0.783	0.756	
ROTOR MOMENTUM RISE EFFICIENCY	0.722	0.722	0.733	0.738	0.731	
ROTOR HEAD RISE COEFFICIENT	0.254	0.231	0.250	0.256	0.258	
FLOW COEFFICIENT HT FLOW PER UNIT FRONTAL AREA HT FLOW PER UNIT ANNULUS AREA	0.351	0.414	0.393	0.380	0.345	
	25.995	29.656	28.744	27.825	26.046	
	35.040	39.974	38.745	37.506	35.108	
HT FLOW AT ORIFICE HT FLOW AT ROTOR INLET HT FLOW AT ROTOR OUTLET	55.058	62.811	60.880	58.933	55.165	
	55.542	62.895	60.670	59.083	54.671	
	52.016	59.062	56.477	55.227	52.425	
RPM PERCENT OF DESIGN SPEED	16035.067	16030.468	16026.682	16010.855	15999.836	
	100.219	100.190	100.167	100.068	99.999	

TABLE V. - Concluded. OVERALL PERFORMANCE FOR ROTOR 5 WITH DIFFERENT ROTOR CASINGS

(d) With shallow, short blade-angle slot casing

		Reading	number	
	761-1629	762-1640	763-1651	764-1662
ROTOR TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENCY ROTOR HEAD RISE COEFFICIENT FLOW COEFFICIENT WIF FLOW PER UNIT FRONTAL AREA WIF FLOW PER UNIT ANNULUS AREA WIF FLOW AT ORIFICE WIF FLOW AT ROTOR INLET HIF FLOW AT ROTOR OUTLET RPM PERCENT OF DESIGN SPEED	1.866 1.240 0.812 0.807 0.322 0.354 26.117 35.204 55.317 55.994 52.776 15987.962 99.925	1.758 1.208 0.841 0.823 0.287 0.426 29.958 40.381 63.451 64.390 61.015 16015.620 100.098	1.859 1.230 0.842 0.831 0.318 0.394 28.666 38.640 60.716 60.791 57.181 16025.916	1.872 1.241 0.813 0.806 0.322 0.353 26.400 35.586 55.916 55.952 52.902 16023.144

(e) With skewed slot casing

		Reading	number	
	508-924	510-940	511-951	512-962
ROTOR TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY ROTOR MEMENTUM RISE EFFICIENCY ROTOR HEAD RISE COEFFICIENT FLOW COEFFICIENT HT FLOW PER UNIT FRONTAL AREA HT FLOW PER UNIT ANNULUS AREA HT FLOW AT ROTOR INLET HT FLOW AT ROTOR OUTLET RPM PERCENT OF DESIGN SPEED	1.896 1.257 0.780 0.864 0.328 0.353 26.630 35.896 56.403 55.966 53.913 16049.437	1.792 1.233 0.778 0.872 0.294 0.410 29.894 40.295 63.316 62.677 60.761 16124.841	1.901 1.257 0.786 0.876 0.327 0.374 27.951 37.675 59.199 58.509 57.338 16121.884	1,909 1,262 0,774 0,857 0,329 0,349 26,436 35,634 55,992 55,325 54,107 16121,531 100,760

(f) With circumferentially grooved casing

		Reading	number	
	602-1227	603-1238	604-1249	605-1260
ROTOR TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENCY ROTOR HEAD RISE COEFFICIENT FLOW COEFFICIENT HT FLOW PER UNIT FRONTAL AREA HT FLOW PER UNIT ANNULUS AREA HT FLOW AT ROTOR INLET HT FLOW AT ROTOR OUTLET RPM PERCENT OF DESIGN SPEED	1.867 1.233 0.839 0.835 0.322 0.377 27.331 36.840 57.886 58.765 55.861 15996.219 99.976	1.755 1.201 0.869 0.852 0.287 0.439 30.547 41.175 64.698 65.470 63.080 15997.943 99.987	1.857 1.225 0.860 0.855 0.319 0.404 28.838 38.871 61.079 61.748 59.072 15989.649 99.935	1.864 1.232 0.840 0.838 0.322 0.378 27.493 37.058 58.230 58.685 56.053 15973.580 99.835

TABLE VI. - BLADE-ELEMENT DATA AT BLADE EDGES FOR SOLID CASING

(a) Reading number, 443-684

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	9.531 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.4 1.6 1.6 1.6 1.7 1.5 1.5	BETAM OUT 55.0 47.0 48.8 48.9 49.3 48.9 47.0 47.6 47.6	REL IN 65.5 64.1 58.3 56.0 55.4 54.4 54.1 50.5	BETAM OUT 56.4 46.5 45.8 46.4 46.2 44.7 43.5 35.1 27.0 20.7	TOTA IN 520.7 520.0 519.4 518.9 518.9 518.4 518.2 517.7 517.3	RATIO 1.276 1.257 1.232 1.219 1.214 1.210 1.207 1.203 1.177	TOTAL IN 14.52 14.66 14.72 14.71 14.71 14.72 14.71 14.73	PRESS RATIO 1.914 1.902 1.822 1.782 1.766 1.765 1.774 1.716 1.673
RP 1 2 3 4 5 6 7 8 9 10 11	ABS IN 608.8 634.5 733.4 758.8 765.1 766.5 768.0 766.3 700.9 630.7 610.8	VEL 0UT 796.1 804.7 833.6 809.7 791.4 787.7 795.0 800.2 813.6 827.8 866.9	REL IN 1469.0 1454.0 1393.4 1356.3 1345.9 1334.5 1319.0 1307.1 1146.9 1004.0 959.3	VEL OUT 825.5 859.5 825.6 765.4 754.5 742.7 734.7 678.0 626.6 606.6	MERI IN 608.6 634.3 733.1 758.5 764.8 766.2 767.6 766.0 700.7 630.5 610.6	D VEL 0UT 456.8 510.6 568.6 533.4 520.0 514.0 552.5 533.0 554.9 558.4 567.6	TAN IN 15.4 15.8 20.5 21.0 21.4 22.2 19.8 15.1 13.8	G VEL 0UT 652.0 621.9 609.6 609.1 596.6 596.8 599.2 596.9 595.1 611.1 655.2	IN	1208.2 1158.1 1143.4 1131.9 1115.7
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M 1N 0.561 0.587 0.713 0.720 0.721 0.723 0.722 0.655 0.565	ACH NO OUT 0.657 0.670 0.705 0.687 0.672 0.669 0.684 0.705 0.724 0.757	REL M/ IN 1.354 1.345 1.305 1.275 1.266 1.256 1.242 1.231 1.072 0.931 0.887	OUT 0.681 0.716 0.698 0.650 0.640 0.631 0.626 0.628 0.588 0.548	MERID M 1N 0.561 0.587 0.687 0.713 0.720 0.721 0.721 0.655 0.565	ACH NO OUT 0.377 0.425 0.481 0.453 0.441 0.455 0.455 0.481 0.488 0.495				PEAK SS MACH NO 1.642 1.630 1.557 1.503 1.489 1.461 1.467 1.460 1.413
RP 1 2 3 4 5 6 7 8 9	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 4.0 3.6 2.0 1.7 1.6 1.7 1.8 1.9 4.7 6.4 6.5	DENCE SS 1.7 1.0 -1.9 -2.6 -2.8 -2.8 -2.9 -1.2 -0.2	7.6 5.3 1.5 3.5 4.9 4.6 5.9 7.9	D-FACT 0.579 0.542 0.532 0.558 0.558 0.562 0.561 0.556 0.527 0.498 0.498	0.737 0.788 0.869 0.855 0.839 0.840 0.852 0.875 0.942 0.976	LOSS CO TOT 0.275 0.214 0.131 0.143 0.156 0.155 0.145 0.122 0.061 0.030 0.112	OEFF PROF 0.170 0.114 0.053 0.080 0.098 0.099 0.093 0.074 0.038 0.028 0.111	LOSS P TOT 0.050 0.041 0.026 0.028 0.030 0.029 0.023 0.011 0.005 0.019	ARAM PROF 0.031 0.022 0.011 0.016 0.019 0.019 0.018 0.014 0.007 0.005 0.019

TABLE VI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SOLID CASING

(b) Reading number, 444-695

			•	•	.g	-				
RP	RAD IN	II OUT	ABS IN	BETAM	REL IN	BETAM	TOTA IN	L TEMP	IN	PRESS RATIO
1	9.622	9.531	1.3	37.2	64.1	55.0	520.8	1.191	14.62	1.537
2	9.426	9.349	1.4	33.3	63.3	53.7	520.0	1.173	14.64	1.564
3 4	8.587 8.152	8.607 8.239	1.7 1.7	34.8 35.3	57.8 55.3	48.2 52.0	519.1 518.8	1,174	14.66	1.554
5	8.040	8.146	1.5	35.5	54.8	51.8	519.0	1,144	14.69	1.355
6	7.927	8.054	1.5	35.7	54.2	50.5	518.5	1.145	14.70	1.363
7	7.800	7,949	1.6	35.8	53.8	48.4	518.3	1.146	14.70	1.390
8 9	7.700 6.611	7.868 7.025	1.5 1.7	35.5 34.9	53.6 51.4	46.6 37.4	518.3 517.4	1.148	14.72 14.73	1.417
10	5.681	6.387	1.5	38.4	50.0	26.4	517.8	1.147	14.75	1.574
11	5.377	6.201	1.4	40.5	49.3	21.6	518.2	1.159	14.75	1.595
	ABS	VEL	REL	VEL	MERI	D VEL	TAN	G VEL	WHEEL	SPEED
RP	IN	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT
1	648.3	769.3	1485.7		648.1	612.5	15.1	465.5	1351.9	
2 3	656. 3 744.7	778.3 811.4	1462.5 1397.8	1098.0 998.9	656.1 744.4	650.5 666.2	15.7 21.6	427.3 463.2	1322.8	
Ã	774.5	711.9	1360.6	942.6	774.2	580.8	23.0	411.6	1141.8	
5	782.7	707.3	1356.2	931.8	782.5	575.8	20.6	410.7	1128.4	
6 7	786.5	721.0	1345.4	919.8	786.2	585.4	20.8	420.8	1112.5	
É	784.1 783.2	743.8 765.9	1328.5 1318.4	908.8 908.3	783.8 782.9	603.1 623.8	21.8 20.3	435.4 444.4	1094.4	
9	724.7	822.8	1160.8	849.6	724.4	675.1	20.9	470.2	927.9	986.0
10	655.4	888.8	1019.6	777.4	655.2	696.4	17.2	552.3	798.4	897.7
11	635.8	916.5	975.1	749.7	635.6	697.1	15,7	595.0	755.2	870.9
RP	IN ABS M	ACH NO OUT	REL M	ACH NO OUT	MERID M	ACH NO OUT				PEAK SS
t	0.600	0.657	1.375	0.911	0.600	0.523			0.945	MACH NO 1.616
2	0.608	0.671	1.356	0.947	0.608	0.561			0.991	1.615
3 4	0.699 0.730	0.703 0.619	1.311	0.865 0.819	0.698 0.729	0.577 0.505			0.895 0.750	1.548
5	0.738	0.614	1.279	0.809	0.738	0.500			0.736	1.480
5 6	0.743	0.627	1.270	0.800	0.742	0.509			0.745	1.469
7	0.740	0.648	1.254	0.792	0.740	0.525			0.769	1.458
8 9	0.739 0.679	0.669 0.728	1.244	0.793 0.752	0.739 0.679	0.545 0.597			0.797 0.932	1.453
10	0.609	0.789	0.947	0.690	0.609	0.618			1.063	1.238
11	0.589	0.812	0.904	0.664	0.589	0.617			1.097	1.178
	PERCENT		IDENCE	DEV	D-FACT	EFF	LOSS C		LOSS P	
RP	SPAN	MEAN		٠.			TOT	PROF	TOT	PROF
1 2	7.00 11.70	2.6 2.8		6.1 5.5	0.380 0.339	0.683 0.785	0.244	0.142	0.046 0.030	0.027
3	30.90	1.5		3.1	0.378	0.771	0.177	0.100	0.035	0.020
4	40.40	1.1	-3.2	9.7	0.388	0.655	0.231	0.171	0.040	0.029
5	42.80	1.0		10.3	0.393	0.630	0.248	0.189	0.042	0.032
6 7	45.20 47.90	1.0 1.2		9.8 8.7	0.398 0.400	0.638 0.673	0.247 0.230	0.191 0.179	0.043	0.033
8	50.00	1.4	-3.4	7.7	0.397	0.709	0.210	0.161	0.038	0.029
9	71.80	3.7	-2.2	8.2	0.359	J.871	0.107	0.085	0.019	0.015
10	88.30	5.3		7.3	0.345	0.939	0.067	0.065	0.012	0.011
11	93.10	5.3	-1.4	6.0	0.347	0.897	0.131	0.130	0.022	0.022

TABLE VI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SOLID CASING

(c) Reading number, 445-706

			V	c) Itcaui	u	,01, 440	-100			
RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	9.531 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.4 1.7 1.8 1.6 1.6 1.5 1.6	BETAM OUT 53.6 48.0 45.1 47.3 47.4 47.3 46.9 46.3 45.1 45.8	REL IN 64.7 64.0 58.5 56.2 55.7 55.2 54.3 52.2 50.9	BETAM OUT 56.8 53.3 46.7 46.7 46.4 45.0 43.7 35.2 27.4 20.9	TOTA IN 520.4 519.6 518.6 518.3 518.3 518.3 518.2 518.2 518.3	AL TEMP RATIO 1.263 1.245 1.230 1.215 1.208 1.205 1.205 1.198 1.175 1.162	TOTAL IN 14.65 14.65 14.66 14.67 14.68 14.69 14.70 14.73 14.73	PRESS RAT10 1.832 1.867 1.890 1.794 1.747 1.727 1.728 1.739 1.694 1.659
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 630.5 637.2 728.7 754.4 757.2 760.0 760.5 761.3 704.7 633.1 613.7	VEL 0UT 782.2 799.8 840.7 811.2 788.0 782.6 789.3 816.9 830.9 873.4	REL IN 1476.8 1454.5 1392.7 1353.7 1343.7 1316.0 1305.1 1149.6 1004.0 962.4	VEL 0UT 846.6 894.9 855.0 787.4 777.8 769.6 762.6 763.0 706.4 653.1 627.2	MERI 1N 630.3 728.3 754.0 756.9 759.7 760.2 761.1 704.5 632.8 613.6	D VEL 0UT 463.6 534.7 593.4 550.0 533.4 530.8 538.9 551.9 576.9 579.6 586.1	TAN IN 15.6 15.7 21.3 23.3 20.9 21.8 21.1 20.4 19.4 17.6	G VEL 0UT 630.0 594.8 595.6 596.3 580.0 575.1 576.7 576.7 576.7 576.7	HHEEL 1351.1 1323.2 1208.4 1147.5 1131.1 1114.6 1095.2 1080.5 927.9 797.3 755.1	1312.4 1211.3 1159.8 1146.1 1132.4 1116.2
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M. IN 0.583 0.590 0.683 0.709 0.712 0.715 0.715 0.716 0.658 0.586	ACH NO OUT 0.648 0.670 0.713 0.690 0.671 0.667 0.667 0.674 0.683 0.709 0.726 0.762	REL M. 1N 1.365 1.346 1.305 1.273 1.264 1.252 1.238 1.228 1.074 0.930 0.889	ACH NO OUT 0.701 0.749 0.725 0.670 0.662 0.656 0.651 0.653 0.613 0.571	MERID M 1N 0.582 0.590 0.682 0.709 0.712 0.715 0.715 0.716 0.658 0.586 0.567	OUT 0.384 0.448 0.503 0.468 0.454 0.452 0.462 0.472 0.500 0.507 0.511				PEAK SS MACH NO 1.626 1.628 1.564 1.506 1.498 1.486 1.473 1.465 1.410
RP 1 2 3 4 5 6 7 B 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC I MEAN 3.2 3.5 2.2 1.9 2.0 2.1 4.5 6.2	DENCE SS 0.9 0.9 -1.6 -2.4 -2.5 -2.6 -2.6 -2.7 -1.3 -0.4 -0.3	8.0 5.1 1.0 3.4 5.2 5.7 5.3 4.8 6.1 8.4 5.3	D-FACT 0.562 0.512 0.507 0.537 0.537 0.536 0.535 0.530 0.500 0.468 0.477	0.718 0.799 0.868 0.846 0.832 0.823 0.823 0.844 0.864 0.931 0.962	LOSS CO TOT 0.281 0.197 0.131 0.149 0.160 0.168 0.148 0.130 0.072 0.046 0.127	DEFF PROF 0.178 0.097 0.052 0.086 0.100 0.112 0.096 0.081 0.049 0.044 0.127	LOSS P. TOT 0.050 0.038 0.027 0.029 0.030 0.032 0.028 0.025 0.013 0.008 0.022	ARAM PROF 0.032 0.019 0.017 0.017 0.019 0.021 0.016 0.009 0.009

TABLE VI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES $\mbox{FOR SOLID CASING}$

(d) Reading number, 477-830

RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10
PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	ABS M. IN 0.558 0.582 0.674 0.707 0.708 0.710 0.709 0.650 0.581 0.556	ABS IN 605.3 629.7 720.3 748.5 752.4 753.2 754.9 754.1 696.4 627.3 602.8	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377
INC MEAN 4.0 3.7 2.2 2.1 2.0 2.2 4.8 6.7	ACH NO OUT 0.664 0.674 0.706 0.686 0.676 0.672 0.678 0.690 0.702 0.719 0.755	VEL 0UT 802.2 806.8 834.3 807.9 795.9 790.6 795.0 807.2 810.5 825.3 867.2	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201
IDENCE SS 1.7 1.1 -1.6 -2.2 -2.4 -2.5 -2.4 -1.0 0.1	REL M IN 1.344 1.340 1.291 1.268 1.258 1.242 1.234 1.223 1.067 0.930 0.878	REL IN 1457.4 1448.8 1379.5 1350.3 1338.8 1321.5 1312.3 1301.6 1143.8 1005.1 951.1	ABS IN 1.6 0.9 1.8 1.0 1.2 1.6 1.2 1.1
DEV 6.6 5.0 1.2 3.3 4.4 4.9 4.7 3.8 5.9 7.9 4.6	ACH NO OUT 0.681 0.703 0.686 0.627 0.618 0.612 0.640 0.586 0.547 0.520	VEL 0UT 822.5 841.7 810.2 749.3 738.2 726.5 717.9 748.6 676.9 628.0 597.1	BETAM OUT 54.4 51.4 47.7 49.5 49.8 50.0 49.8 47.1 46.9 47.3 49.7
D-FACT 0.578 0.555 0.539 0.570 0.572 0.572 0.575 0.543 0.543 0.497 9.505	MERID M IN 0.558 0.582 0.674 0.703 0.707 0.708 0.710 0.709 0.650 0.581 0.556	MERI IN 605.1 629.6 748.4 752.3 752.9 754.8 754.8 696.2 627.3	REL IN 65.5 64.2 58.5 56.3 55.8 55.8 54.6 52.5 51.4 50.7
0.753 0.799 0.871 0.850 0.840 0.837 0.852 0.813 0.929 0.935 0.905	OUT 0.386 0.421 0.475 0.446 0.437 0.432 0.437 0.430 0.488	D VEL OUT 466.4 503.8 661.1 524.6 513.9 508.2 513.0 549.7 554.0 559.6 560.7	BETAM 0UT 55.4 53.2 46.2 45.6 45.9 45.6 44.4 42.7 35.1 27.0 20.1
LOSS C TOT 0.258 0.202 0.130 0.148 0.156 0.160 0.145 0.181 0.076 0.082 0.139		TAN IN 16.8 10.4 22.4 13.4 15.2 14.6 15.3 75.8	TOTA IN 519.7 519.5 518.6 518.6 518.7 518.4 518.5 518.4 518.6
OEFF PROF 0.157 0.153 0.055 0.085 0.098 0.106 0.093 0.131 0.053 0.053		652.6 630.2 617.4 614.4 607.7 605.6 607.3 591.0 606.6 661.5	L TEMP RATIO 1.272 1.253 1.231 1.217 1.213 1.210 1.206 1.202 1.177 1.168 1.180
LOSS P TOT 0.048 0.039 0.026 0.029 0.030 0.030 0.030 0.035 0.014 0.014		WHEEL 1342.7 1315.2 1199.1 1137.3 1122.8 1107.1 1088.8 1075.6 922.8 793.1 751.7	TOTAL IN 14.53 14.66 14.71 14.72 14.72 14.72 14.72 14.72 14.72 14.72
PROF 0.029 0.020 0.011 0.017 0.019 0.020 0.018 0.026 0.014 0.024	PEAK SS MACH NO 1.631 1.629 1.553 1.509 1.496 1.479 1.476 1.470 1.417	1304.4 1201.9 1149.4 1137.6 1124.8 1109.6	PRESS RAT10 1.918 1.907 1.901 1.809 1.781 1.763 1.762 1.702 1.704 1.665 1.695

(e) Reading number, 478-847

			·	-,		,				
RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	9.531 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.6 1.0 1.5 1.5 1.1 1.0 1.0 1.1	0UT 33.2 31.0 31.9 32.7 32.2 32.6 32.5 32.6 32.5 37.4	REL IN 64.3 62.9 56.9 54.3 53.3 53.0 52.6 49.8 49.3	BETAM 0UT 55.2 53.5 49.0 52.2 52.1 50.8 48.6 47.0 37.7 21.6	TOTA IN 519.7 519.6 518.5 518.5 518.5 518.4 518.4 518.4 518.5	AL TEMP RAT10 1.167 1.159 1.157 1.129 1.129 1.131 1.133 1.135 1.136	TOTAL IN 14.48 14.65 14.72 14.72 14.72 14.72 14.73 14.72 14.71	PRESS RAT10 1.486 1.497 1.467 1.300 1.290 1.350 1.357 1.441 1.570
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 637.8 668.5 769.5 802.4 811.7 809.0 810.0 744.3 662.5 635.5	VEL 0UT 760.8 779.1 798.8 709.0 703.6 716.6 743.1 762.7 824.8 889.7 920.6	IN 1471.3	1123.3	MERI IN 637.6 668.4 769.3 802.1 811.6 813.9 809.8 809.8 744.2 662.4 635.4	D VEL 0UT 636.7 667.7 678.5 596.8 595.6 603.8 626.4 642.4 710.6 711.5	TAN IN 18.2 11.8 19.7 21.7 15.4 14.6 15.5 16.1 11.1	G VEL OUT 416.5 401.5 421.6 382.7 374.6 385.8 399.8 411.1 442.8 535.4 584.2	WHEEL 1344.2 1315.6 1199.0 1139.0 1124.7 1107.3 1089.9 1076.1 922.8 794.1 751.3	1304.8 1201.8 1151.1 1139.6 1125.1 1110.7
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M. IN 0.590 0.621 0.725 0.769 0.771 0.766 0.767 0.699 0.616 0.589	ACH NO OUT 0.657 0.677 0.697 0.620 0.615 0.627 0.652 0.670 0.732 0.732	REL M. 1N 1.362 1.361 1.301 1.302 1.291 1.274 1.264 1.101 0.953 0.904	ACH NO OUT 0.962 0.976 0.902 0.851 0.848 0.835 0.831 0.827 0.780 0.706	MERID M. IN 0.590 0.621 0.724 0.759 0.769 0.769 0.767 0.699 0.616 0.589	ACH NO 0.550 0.580 0.592 0.522 0.522 0.521 0.528 0.549 0.564 0.617 0.630 0.630				PEAK SS MACH NO 1.609 1.603 1.530 1.470 1.459 1.458 1.449 1.437 1.237
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC I MEAN 2.8 2.3 0.1 0.1 0.1 0.4 2.9 5.0	DENCE SS 0.5 -0.3 -3.2 -4.2 -4.4 -4.5 -4.3 -4.4 -2.9 -1.5 -1.3	DEV 6.3 5.3 4.0 9.9 10.6 10.1 8.9 8.0 8.6 7.6	D-FACT 0.330 0.318 0.350 0.366 0.367 0.374 0.373 0.374 0.336 0.329 0.330	0.716 0.767 0.736 0.604 0.583 0.594 0.640 0.678 0.847 0.891	LOSS COTOT 0.200 0.159 0.184 0.237 0.250 0.248 0.210 0.119 0.1175	DEFF PROF 0.102 0.062 0.177 0.190 0.176 0.161 0.098 0.116 0.175	LOSS P. TOT 0.037 0.036 0.041 0.042 0.043 0.043 0.038 0.021 0.020 0.030	ARAM PROF 0.019 0.012 0.031 0.032 0.033 0.031 0.029 0.018 0.020 0.029

TABLE VI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SOLID CASING

(f) Reading number, 479-858

			-	•	-B	,				
RP 1 2	RAD IN 9.622 9.426	0UT 9.531 9.349	ABS [N 1.6 1.4	BETAM OUT 51.5 47.3	REL IN 64.8 63.2	0UT 56.5 53.4	TOTA IN 519.9 519.3	RAT10 1.248 1.232	TOTAL IN 14.50 14.66	PRESS RATIO 1.798 1.804
3	8.587	8.607	1.5	44.3	57.4	45.4	518.4	1.221	14.72	1.844
4	8.152 8.040	8.239 8.146	1.6 1.4	46.3 46.9	54.8 54.3	46.0 46.6	518.6 518.5	1.203	14.72 14.72	1.728
6	7.927	8.054	1.1	46.4	53.9	46.5	518.5	1.194	14.72	1.670
7	7.800 7.700	7.949 7.868	1.3	46.2 44.9	53.4 53.0	45.2 43.9	518.4 518.4	1.190	14.72	1.676 1.693
9	6.611	7.025	1.2	43.6	51.2 50.3	35.6	518.6 518.3	1.167	14.72	1.656 1.632
10 11	5.681 5.377	6.387 6.201	1.2	44.9 47.0	49.9	27. 3 20.8	518.6	1.175	14.70	1.667
00		VEL		VEL		D VEL		IG VEL		SPEED
RP 1	(N 626.6	0UT 773.1	IN 1468.6	0UT 872.5	IN 626.4	0UT 481.2	(N 17.3	0UT 605.1	IN 1345.6	0UT 1332.9
2 3	656.7 755.9	792.2 845.8	1457.3	902.2	656.5 755.7	537.6 605.2	16.1 19.3	581.9 590.9	1317.1	1306.4
4	789.8	800.9	1369.4	796.8	789.5	553.0	21.8	579.3	1140.7	1152.9
5 6	796.3 797.3	784.3 776.2	1363.1 1353.4	780.9 777.9	796.1 797.1	536.1 535.4	18.9 14.8	572.5 562.0	1125.4	1140.3
7	797.0	783.5	1336.6	770.0	796.8	542.7	17.5	565.1	1090.6	1111.4
8 9	798.1 730.5	793.6 813.6	1327.1 1166.3	779.9 72 4. 7	797.9 730.3	561.9 589.5	17.2 15.1	560.3 560.7	1077.7 924.4	1101.2 982.3
10	648.5	833.8	1015.3	664.4	648.4	590.5	13.0	588.6	794.3	893.0
11	622.6	875.5	966.8	638.8	622.5	597.1	12.3	640.3	752.0	867.3
	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO			MERID	PEAK SS
RP 1	IN 0.579	0UT 0.644	IN 1,357	0UT 0.727	IN 0.579	0UT 0.401				MACH NO 1,619
2	0.609	0.667	1.352	0.759	0.609	0.452			0.819	1.607
3 4	0.711 0.746	0.721	1.319	0.734 0.681	0.710 0.746	0.516 0.472			0.801	1.542 1.479
5	0.753	0.670	1.289	0.667	0.753	0.458			0.673	1.472
6 7	0.754 0.754	0.664 0.672	1.280	0.665 0.660	0.754 0.753	0.458 0.465			0.672	1.467 1.452
8	0.755	0.682	1.255	0.670	0.755	0.483			0.704	1.445
9 10	0.684 0.602	0.708 0.729	1.093	0.631 0.581	0.684 0.602	0.513 0.516			0.807 0.911	1.388
11	0.576	0.765	0.894	0.558	0.576	0.52?			0.959	1.184
				55.1						
RP	PERCENT SPAN	INC	IDENCE SS	DEA	D-FACT	EFF	LOSS C	PROF	LOSS F	PROF
1	7.00	3.3	1.0	7.7	0.536	0.737	0.253	0.153	0.046	0.028
2 3	11.70 30.90	2.7 1.1	0.1 -2.7	5.2 0.4	0.505 0.506	0.790 0.865	0.196 0.128	0.100 0.051	0.037 0.026	0.019
4 5	40.40	0.5 0.5	-3.8 -3.9	3.7 5.1	0.533	0.834	0.151 0.163	0.090	0.029	0.018
6	42.80 45.20	0.7	-3.9	5.8	0.536	0.812	0.167	0.111	0.031	0.021
7 B	47.90 50.00	0.8 0.8		5.5 5.0	0.535 0.522	0.837 0.864	0.145	0.094	0.027	0.018 0.014
9	71.80	3.6	-2.3	6.4	0.489	0.931	0.068	0.046	0.013	0.009
10 11	88.30 93.10	5.6 5.9		8.2 5.3	0.462 0.466	0.929 0.899	0.085 0.140	0.083 0.140	0.015 0.024	0.014

TABLE VI. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES $\mbox{FOR SOLID CASING}$

(g) Reading number, 482-869

RP 1 2 3 4 5 6 7 8 9 10	RAI IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.948 7.868 7.025 6.387 6.201	ABS IN 1.5 1.9 1.6 1.4 1.5 1.4 1.5 1.2	BETAM OUT 54.7 51.2 47.2 49.2 49.8 49.7 49.4 48.6 46.7 47.5	REL IN 65.6 64.1 58.4 56.1 55.6 55.2 54.7 54.4 51.0	BETAM OUT 56.1 53.4 46.1 45.5 46.1 45.7 44.5 43.3 35.1 27.0 20.3	TOT/ 1520.1 519.3 518.8 518.4 518.5 518.3 518.3 518.4 518.4	RATIO 1.271 1.253 1.230 1.217 1.211 1.208 1.204 1.204 1.177 1.168 1.180	TOTA IN 14.49 14.65 14.72 14.72 14.72 14.73 14.73 14.73	1.900 1.895 1.807 1.773 1.756 1.755 1.764 1.706
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 602.7 630.9 726.1 752.6 757.8 757.2 760.0 758.7 697.4 623.3 598.7	VEL OUT 794.6 805.5 836.1 809.6 795.1 789.2 795.1 801.6 811.6 825.2 867.1	REL IN 1459.8 1441.6 1385.1 1349.8 1341.6 1325.2 1314.0 1302.1 1149.1 1000.6 951.0	VEL OUT 823.6 846.0 818.8 754.8 740.3 731.3 725.3 725.3 680.1 625.5 601.3	MERI IN 602.5 630.5 725.8 752.4 757.6 756.9 759.8 759.5 697.3 623.2 598.6	D VEL 0UT 459.0 504.5 568.2 528.8 513.7 517.5 517.5 529.8 556.2 557.2 564.1	TAN IN 15.6 21.4 20.4 18.8 17.9 20.1 18.7 18.3 11.3	G VEL OUT 648.7 627.9 613.4 613.0 606.9 601.9 601.5 591.1 608.6 658.6	IN 1345.3 1317.8 1200.1 1139.5 1125.1 1107.9 1090.8	SPEED 0UT 1332.6 1307.0 1202.9 1151.6 1139.9 1125.6 1111.6 1100.7 982.5 892.8 867.0
RP 1 2 3 4 5 6 7 8 9 10	ABS M. IN 0.556 0.584 0.680 0.707 0.713 0.712 0.715 0.714 0.651 0.577 0.553	ACH NO OUT 0.657 0.673 0.708 0.678 0.676 0.672 0.678 0.678 0.703 0.719	REL M. 1N 1.346 1.297 1.269 1.261 1.246 1.236 1.235 1.072 0.926 0.878	OUT 0.681 0.707 0.694 0.642 0.630 0.623 0.619 0.622 0.523 0.523	MERID M. IN 0.555 0.583 0.679 0.707 0.712 0.712 0.713 0.651 0.577 0.552	OUT 0.380 0.421 0.481 0.450 0.450 0.437 0.435 0.442 0.481 0.481				PEAK SS MACH NO 1.637 1.618 1.554 1.502 1.493 1.479 1.471 1.463 1.424 1.257 1.195
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 4.1 3.5 2.1 1.9 1.9 2.0 2.2 5.0 6.7 7.0	DENCE SS 1.8 0.9 -1.7 -2.4 -2.5 -2.6 -2.7 -2.6 -0.9 0.2 0.3	7.3 5.2 1.0 3.2 4.5 5.1 4.8 4.4 6.0 8.0	D-FACT 0.577 0.547 0.565 0.565 0.569 0.569 0.561 0.527 0.497 0.500	0.747 0.795 0.871 0.851 0.841 0.839 0.839 0.873 0.931 0.934	LOSS CO TOT 0.262 0.207 0.129 0.146 0.154 0.155 0.143 0.124 0.073 0.084 0.141	PROF 0.160 0.111 0.053 0.085 0.095 0.101 0.075 0.049 0.082 0.141	LOSS P TOT 0.048 0.040 0.026 0.029 0.029 0.030 0.027 0.024 0.014 0.015	PROF 0.029 0.021 0.011 0.017 0.018 0.019 0.018 0.015 0.009 0.014

TABLE VII. -BLADE-ELEMENT DATA AT BLADE EDGES FOR DEEP, LONG BLADE-

ANGLE SLOT CASING

(a) Reading number, 551-1061

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.377	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.868 7.025 6.387 6.201	ABS IN 4.1 3.8 3.4 2.65 2.0 1.8 1.5 1.4	BETAM OUT 69.9 60.8 44.3 43.7 45.0 45.1 45.5 42.5 43.8 45.5	REL 1N 71.7 70.4 64.9 62.0 61.3 60.9 60.4 56.2 54.6 54.0	BETAM 0UT 75.6 68.6 50.4 46.8 45.8 44.2 41.2 39.9 32.8 24.0 18.7	TOTA IN 521.5 520.7 520.3 518.8 518.1 517.6 517.7 517.5 517.5	TEMP RATIO 1.322 1.290 1.198 1.195 1.199 1.202 1.205 1.207 1.174 1.169 1.179	TOTAL IN 14.53 14.63 14.68 14.71 14.72 14.73 14.72 14.73 14.73	PRESS RAT10 1.444 1.458 1.633 1.634 1.625 1.638 1.663 1.665 1.669 1.674 1.699
RP 1 2 3 4 5 6 7 8 9 10	ABS !N 436.0 460.9 548.2 592.3 601.7 607.1 610.2 6098.4 556.8 536.7	VEL OUT 586.3 617.2 771.3 789.2 794.5 807.9 830.0 846.9 854.5 883.8 913.9	REL IN 1385.8 1369.2 1291.3 1261.6 1252.8 1246.2 1233.5 1224.2 1094.6 960.9 911.7	VEL 0UT 809.3 827.7 865.9 865.9 806.5 795.7 778.2 778.2 749.0 698.1 676.4	MERI IN 434.8 459.9 547.7 601.1 606.7 609.9 609.6 608.2 556.6 536.5	D VEL OUT 201.6 301.4 552.4 571.0 562.0 570.2 580.4 593.2 629.7 637.9 640.7	TAN IN 31.3 30.6 326.8 26.0 21.1 18.9 16.1 15.2	G VEL 0UT 550.6 538.6 538.3 544.8 561.6 572.4 604.5 577.6 611.8 651.7	1347.1 1320.2 1202.2 1141.0 1125.2 1109.7	1309.5 1205.0 1153.2 1140.0 1127.5
RP 1 2 3 4 5 6 7 8 9 10	ABS M IN 0.396 0.419 0.503 0.556 0.556 0.564 0.564 0.563 0.512 0.493	ACH NO OUT 0.465 0.498 0.657 0.676 0.680 0.692 0.712 0.727 0.746 0.802	REL M. 1N 1.257 1.245 1.184 1.163 1.157 1.152 1.141 1.132 1.012 0.884 0.838	ACH NO OUT 0.642 0.668 0.737 0.714 0.690 0.681 0.667 0.664 0.654 0.594	MERID M IN 0.395 0.418 0.546 0.555 0.561 0.564 0.564 0.562 0.512 0.493	ACH NO OUT 0.160 0.243 0.470 0.489 0.481 0.488 0.498 0.509 0.550 0.562				PEAK SS MACH NO 1.762 1.750 1.676 1.612 1.598 1.594 1.585 1.585 1.521 1.227
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 95.10	INC MEAN 10.2 9.8 8.6 7.6 7.6 7.7 7.9 8.6	7.9 7.3 4.8 3.5 3.2 3.1 3.0 3.1 2.7 3.3	DEV 26.8 20.4 5.3 4.5 4.3 3.5 2.1 1.0 3.7 4.9	D-FACT 0.538 0.514 0.445 0.454 0.475 0.483 0.495 0.497 0.436 0.401	0.344 0.393 0.760 0.773 0.748 0.750 0.764 0.777 0.908 0.938 0.914	LOSS C TOT 0.727 0.648 0.229 0.221 0.253 0.253 0.246 0.238 0.103 0.085 0.135	OEFF PROF 0.609 0.534 0.144 0.153 0.186 0.190 0.179 0.071 0.083 0.135	LOSS TOT 0.059 0.076 0.043 0.042 0.048 0.049 0.049 0.049 0.020 0.015	PROF 0.050 0.062 0.027 0.029 0.036 0.037 0.036 0.014 0.015

TABLE VII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR DEEP,

(b) Reading number, 552-1073

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.377	9.531 9.539 8.607 8.239 8.146 8.054 7.948 7.025 6.387 6.201	ABBIN 1.1.6 2.2 1.5 1.5 1.7 1.4 1.7 1.8	5 BETAM OUT 39.4 35.7 37.1 37.9 39.7 40.7 40.8 40.7 38.3 40.2 42.3	RELIN 67.4 65.7 59.6 56.8 56.1 55.7 554.9 48.3 51.2 50.3	BETAM OUT 63.9 60.1 50.5 48.0 47.7 46.2 44.1 42.4 32.3 26.2 20.8	TOTA IN 520.4 519.2 519.0 518.4 518.6 518.3 518.7 518.7	RATIO 1.192 1.163 1.174 1.172 1.174 1.177 1.180 1.179 1.156 1.158	TOTAL IN 14.50 14.65 14.70 14.72 14.72 14.72 14.73 14.73	PRESS RATIO 1.431 1.480 1.559 1.559 1.512 1.513 1.564 1.664 1.674 1.602
RP 1 2 3 4 5 6 7 8 9	ABS IN 557.6 589.8 688.4 734.2 744.4 742.5 739.1 740.0 804.5 627.2 608.1	VEL 0UT 602.9 656.6 766.1 774.0 768.6 781.7 802.2 818.5 880.6 876.6 908.7	REL IN 1448.9 1430.2 1361.4 1341.6 1333.6 1317.3 1303.2 1287.2 1209.9 999.6 952.1		MER1 IN 557.5 589.5 687.9 733.9 744.2 742.1 738.9 739.6 804.2 626.9 607.8	D VEL OUT 466.0 533.4 610.8 610.5 591.1 592.8 607.2 620.4 691.3 669.2 671.6	TAN IN 11.1 16.9 26.9 18.8 19.5 21.7 17.7 22.5 20.9 18.2	G VEL OUT 382.4 382.9 462.4 475.8 491.3 509.6 524.2 533.8 545.4 566.2 612.1	WHEEL IN 1348.5 1320.0 1201.8 1141.9 1126.1 1110.0 1091.2 1076.0 924.8 796.7 752.3	1309.2 1204.6 1154.0 1141.0 1127.8 1112.0
RP 123345 6789 1011	ABS M IN 0.512 0.543 0.641 0.688 0.699 0.697 0.694 0.761 0.581 0.562	ACH NO OUT 0.506 0.562 0.660 0.669 0.663 0.674 0.693 0.776 0.773	REL M IN 1.329 1.318 1.258 1.252 1.236 1.223 1.208 1.145 0.926 0.880	0.891 0.891 0.915 0.758 0.758 0.739 0.730 0.727 0.721 0.658 0.633	MERID M IN 0.511 0.543 0.641 0.688 0.699 0.696 0.696 0.693 0.594 0.761 0.581	ACH NO OUT 0.391 0.457 0.526 0.528 0.510 0.511 0.524 0.537 0.610 0.590				PEAK SS MACH NO 1.681 1.656 1.570 1.516 1.500 1.485 1.468 1.323 1.247
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 47.90 50.00 71.80 88.30 93.10	INC MEAN 5.9 5.1 2.6 2.3 2.5 2.7 0.7 6.3	IDENCE SS 3.6 2.5 -0.5 -1.7 -2.1 -1.9 -2.1 -5.2 -0.1	DEV 15.1 11.9 5.5 5.7 6.2 5.5 4.4 3.4 3.2 7.2	D-FACT 0.351 0.334 0.388 0.416 0.440 0.452 0.457 0.454 0.426 0.366 0.367	0.561 0.727 0.777 0.762 0.721 0.716 0.733 0.764 1.013 0.984	LOSS CO TOT 0.342 0.195 0.179 0.191 0.227 0.239 0.230 0.208 -0.012 0.104 0.160	PROF 0.232 0.093 0.104 0.129 0.169 0.184 0.179 0.161	LOSS P TOT 0.049 0.031 0.033 0.036 0.042 0.044 0.041 -0.002 0.018 0.027	PROF 0.033 0.015 0.019 0.024 0.031 0.035 0.034 0.031

TABLE VII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR DEEP,

(c) Reading number, 553-1084

				• •	_	-				
	RAD			BETAM		BETAM		L TEMP		PRESS
RP	IN	OUT	IN_	OUT	IN	TUO	IN.	RATIO	IN	RATIO
1	9.622	9.531	2.5	47.4	68.8	68.8 63.1	520.4 519.5	1.224	14.49 14.64	1.413
2 3	9.426 8.587	9.349 8.607	2.2 2.5	42.0 41.3	67.3 61.5	49.7	519.5	1.190	14.69	1.620
4	8.152	8.239	1.8	41.0	58.8	47.3	518.3	1.185	14.73	1.592
5	B. 040	8.146	1.6	42.7	58.0	46.7	517.8	1.188	14.73	1.578
ě	7.927	8.054	1.7	43.1	57.5	45.0	518.1	1,191	14.73	1.588
7	7,800	7.949	1.6	43.3	57.1	42.9	518.1	1.193	14.72	1.612
8	7.700	7.868	1.5	43.6	56.9	40.9	518.1	1.194	14.72	1.635
9	6.611	7.025	1,7	40.2	53.5	33.7	518.2	1.165	14.73	1.638
10	5.681	6.387	1.9	41.9	52.2	25.6	518.2	1.163	14.74	1.631
11	5.377	6.201	1.7	44.2	51.7	19.8	518.1	1.175	14.73	1.667
	ABS	VEL	REL	VEL	MER I	D VEL	TAN	G VEL	WHEEL	SPEED
RP	IN	OUT	IN	0UT	IN	OUT	I N	OUT	IN	OUT
1	514.3	537.8	1422.3		513.8	364.3	22.2	395.7	1348.4	
2	544.2	614.4		1007.3	543.7	456.2	21.2	411.5	1320.3	
3 4	638.3	779.6	1337.1	907.0	637.7	586.1	28.3	514.1	1203.5	
4	679.8	782.5	1309.8	870.5	679.4	590.5	20.9 19.6	513.3	1140.7	
5 6	691.0 694.B	782.9 797.3	1304.5	838.9 823.6	690.7 694.5	575.5 582.2	20.3	530.8 544.8	1126.3	
7	693.0	816.7	1276.7	811.5	692.8	594.5	19.1	560.0	1091.5	
8	692.1	835.8	1265.3	801.2	8,169	605.2	18.6	576.4	1078.0	
9	670.7	851.2	1127.4	781.5	670.4	649.9	19.3	549.7	925.7	983.7
10	602.4	872.8	981.9	719.7	602.1	649.2	19.6	583.4	795.2	894.0
11	582.9	911.0	939.3	693.5	582.6	652.7	17.6	635.6	754.5	870.1
	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO			MERID	PEAK SS
RP	[N	OUT	[N	OUT	IN	001				MACH NO
1	0.470	0.443	1.300	0.831	0.470	0.300			0.709	1.702
2 3	0.499	0.517	1.292	0.847	0.499	0.384			0.839	1.687
4	0.591 0.633	0.668 0.673	1.238	0.777 0.748	0.590 0.633	0.502 0.508			0.919	1.606
5	0.645	0.672	1.217	0.720	0.645	0.494			0.833	1.536
6	0.648	0.685	1.206	0.708	0.648	0.500			0.838	1.523
7	0.647	0.702	1,191	0.698	0.646	0.511			0.858	1.516
8	0.646	0.720	1.180	0.690	0.645	0.521			0.875	1.510
9	0.624	0.745	1.049	0.684	0.624	0.569			0.969	1.442
10	0.556	0.767	0.907	0.632	0.556	0.570			1.078	1.253
11	0.537	0.800	0.866	0.609	0.537	0.573			1.120	1.199
	PERCENT	INC	IDENCE	DEV	D-FACT	EFF	LOSS C		LOSS F	
RP	SPAN	MEAN					TOT	PR0F	TOT	PROF
1	7.00	7.3		20.0	0.377	0.463	0.469	0.358	0.055	0.042
2 3	11.70	6.7		14.9	0.373	0.600	0.325	0.220	0.047	0.032
4	30.90	5.2		4.7	0.428	0.777	0.197 0.205	0.119	0.037 0.039	0.023
5	40.40 42.80	4.5 4.3		5.0 5.2	0.466	0.739	0.234	0.173	0.039	0.027
5 6	45.20	4.3		4.3	0.474	0.742	0.237	0.181	0.046	0.035
7	47.90	4,5	-0.2	3.2	0.479	0.756	0.231	0.178	0.045	0.035
8	50.00	4.7		2.0	0.485	0.777	0.215	0.165	0.043	0.033
9	71.80	5.8		4.6	0.417	0.916	0.086	0.062	0.016	0.012
10	88.30	7.4		6.5	0.385	0.922	0.100	0.098	0.017	0.017
11	93.10	7.7	1.0	4.2	0.390	0.900	0.145	0.145	0.025	0.025

TABLE VII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR DEEP,

(d) Reading number, 554-1095

				•						
	RAD			BETAM		BETAM		L TEMP		PRESS
RP	IN	OUT	IN	OUT	IN	OUT	[N	RATIO	IN 14.50	RAT10 1.441
1 2	9.622 9.426	9.531 9.349	3.0 3.2	58.8 49.6	70. 3 68.7	71 .4 65.7	520.9 519.8	1.274	14.64	1.466
3	8.587	8.607	3.0	42.9	63.3	50.0	519.8	1.195	14.68	1.646
4	8.152	8.239	2.1	43.2	58.5	45.1	518.6	1.194	14.72	1.702
5	8.040	8.146	1.9	44.3	59.8	46.2	518.0	1.197	14.73	1.621
5 6 7	7,927	8.054	1.6	44.5	59.3	44.5	517.9	1.199	14.73	1.634
	7.800	7.949	1.7	45.0	58.7	42.1	518.1	1.202	14.73	1.658
8 9	7.700 6.611	7.868 7.025	1.4	45.0 42.0	58.4 54.9	40.3 33.0	518.1 517.6	1.174	14.73	1.672
10	5.681	6.387	1.7	43.2	53.5	24.9	517.9	1.168	14.74	1.658
11	5.377	6.201	1.6	45.0	52.9	19.8	51B.0	1,176	14.73	1.679
	ARC	VEL	PFI	VEL	MERI	D VEL	TAN	G VEL	WHEEL	SPEED
RP	IN	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT
1	473.7	556.7	1403.1	903.8	473.0	288.4	24.6	476.2	1345.5	
2	504.2	596.0	1385.8	937.8	503.4	386.5	27.8	453.7	1319.0	
2 3 4	591.0	775.0	1311.6	883.2	590.2	567.4	30.6	527.9	1201.9	
4	685.4 644.3	815.4 791.4	1310.7 1280.5	841.8 817.8	684.9 644.0	594.2 566.4	25.1 21.0	558.5 552.7	1142.6 1127.7	
5	649.2	805.2	1270.8	804.4	648.9	574.0	17.9	564.7	1110.5	
7	652.4	827.7	1256.5	789.3	652.2	585.7	19.1	584.8	1093.1	
8	654.9	845.6	1250.2	783.3	654.7	597.8	15.5	598.0	1080.6	
9	639.0	856.3	1112.1	758.2	638.8	635.9	18.1	573.6	928.4	986.5
10 11	578.0 558.8	875.7 904.4	970.7 926.4	703.8 679.3	577.8 558.6	638.3 639.0	17.0 15.8	599.6 640.0	797.0 754.8	896.1 870.5
, ,	550.0	304.4	3L0.4	013.3	330.0	035.0	13.0	0-0.0	754.0	610.5
			55. 14		.==					
RP	ABS M	ACH NO OUT	REL M	ACH NO OUT	MERID M. IN	ACH NO OUT				PEAK SS
1	0,431	0.450	1.277	0.730	0.431	0.233			0.610	1.731
2	0.461	0.493	1.266	0.776	0.460	0.320			0.768	1.711
3	0.544	0.661	1.208	0.754	0.544	0.484			0.961	1.639
4	0.030		1.221	0.723	0.638	0.511				
_	0.639	0.701							0.868	1.540
5	0.598	0.677	1.188	0.700	0.598	0.485			0.880	1.571
5 6 7	0.598 0.603	0.677 0.690	1.188 1.180	0.700 0.689	0.598 0.602	0.485 0.492			0.880 0.885	1.571 1.563
7	0.598 0.603 0.606	0.677 0.690 0.710	1.188 1.180 1.167	0.700 0.689 0.677	0.598 0.602 0.606	0.485 0.492 0.502			0.880 0.885 0.898	1.571 1.563 1.550
7 8	0.598 0.603	0.677 0.690	1.188 1.180	0.700 0.689	0.598 0.602	0.485 0.492			0.880 0.885	1.571 1.563
7 8 9 10	0.598 0.603 0.606 0.608 0.593 0.533	0.677 0.690 0.710 0.726 0.747 0.768	1.188 1.180 1.167 1.161 1.032 0.895	0.700 0.689 0.677 0.673 0.662 0.617	0.598 0.602 0.606 0.608 0.593 0.532	0.485 0.492 0.502 0.513 0.555 0.560			0.880 0.885 0.898 0.913 0.995 1.105	1.571 1.563 1.550 1.548 1.483 1.277
7 8 9	0.598 0.603 0.606 0.608 0.593	0.677 0.690 0.710 0.726 0.747	1.188 1.180 1.167 1.161 1.032	0.700 0.689 0.677 0.673 0.662	0.598 0.602 0.606 0.608 0.593	0.485 0.492 0.502 0.513 0.555			0.880 0.885 0.898 0.913 0.995	1.571 1.563 1.550 1.548 1.483
7 8 9 10	0.598 0.603 0.606 0.608 0.593 0.533	0.677 0.690 0.710 0.726 0.747 0.768	1.188 1.180 1.167 1.161 1.032 0.895	0.700 0.689 0.677 0.673 0.662 0.617	0.598 0.602 0.606 0.608 0.593 0.532	0.485 0.492 0.502 0.513 0.555 0.560			0.880 0.885 0.898 0.913 0.995 1.105	1.571 1.563 1.550 1.548 1.483 1.277
7 8 9 10 11	0.598 0.603 0.606 0.608 0.593 0.533	0.677 0.690 0.710 0.726 0.747 0.768 0.793	1.188 1.180 1.167 1.161 1.032 0.895	0.700 0.689 0.677 0.673 0.662 0.617	0.598 0.602 0.606 0.608 0.593 0.532	0.485 0.492 0.502 0.513 0.555 0.560 0.560	LOSS C		0.880 0.885 0.898 0.913 0.995 1.105 1.144	1.571 1.563 1.550 1.548 1.483 1.277 1.217
7 8 9 10 11	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN	0.677 0.690 0.710 0.726 0.747 0.768 0.793	1.188 1.180 1.167 1.161 1.032 0.895 0.852	0.700 0.689 0.677 0.673 0.662 0.617 0.596	0.598 0.602 0.606 0.608 0.593 0.532 0.514	0.485 0.492 0.502 0.513 0.555 0.560 0.560	TOT	PR0F	0.880 0.885 0.898 0.913 0.995 1.105 1.144	1.571 1.563 1.550 1.548 1.483 1.277 1.217
7 8 9 10 11	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN 7.00	0.677 0.690 0.710 0.726 0.747 0.768 0.793 INCI MEAN 8.8	1,188 1,180 1,167 1,161 1,032 0,895 0,852	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV	0.598 0.602 0.606 0.608 0.593 0.532 0.514 D-FACT	0.485 0.492 0.502 0.513 0.555 0.560 0.560	TOT 0.599	PROF 0.485	0.880 0.885 0.898 0.913 0.995 1.105 1.144 LOSS P. TOT 0.062	1.571 1.563 1.550 1.548 1.483 1.277 1.217 ARAM PROF 0.051
7 8 9 10 11	0.598 0.603 0.606 0.608 0.593 0.514 PERCENT SPAN 7.00 11.70	0.677 0.690 0.710 0.726 0.747 0.768 0.793 INCI MEAN 8.8 8.2	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV	0.598 0.602 0.606 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421	0.485 0.492 0.502 0.513 0.555 0.560 0.560	TOT 0.599 0.450	PROF 0.485 0.343	0.880 0.885 0.898 0.913 0.995 1.105 1.144 LOSS P. TOT 0.062 0.059	1.571 1.563 1.550 1.548 1.483 1.277 1.217 ARAM PROF 0.051 0.045
7 8 9 10 11	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN 7.00 11.70 30.90	0.677 0.690 0.710 0.726 0.747 0.768 0.793 INCI MEAN 8.8 8.2 7.0	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6 3.1	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0	0.598 0.602 0.606 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.438	0.485 0.492 0.502 0.513 0.555 0.560 0.560	TOT 0.599	PROF 0.485	0.880 0.885 0.898 0.913 0.995 1.105 1.144 LOSS P. TOT 0.062	1.571 1.563 1.550 1.548 1.483 1.277 1.217 ARAM PROF 0.051
7 8 9 10 11 RP 1 2 3 4 5	0.598 0.603 0.606 0.608 0.593 0.514 PERCENT SPAN 7.00 11.70	0.677 0.690 0.710 0.726 0.747 0.768 0.793 INC MEAN 8.8 8.2 7.0 4.22 6.1	1.188 1.180 1.167 1.161 1.032 0.895 0.852 DENCE SS 6.5 5.6 3.1 -0.1	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6	0.598 0.602 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.472	0.485 0.492 0.502 0.513 0.555 0.560 0.560 EFF 0.402 0.709 0.784 0.751	TOT 0.599 0.450 0.201 0.142 0.238	PROF 0.485 0.343 0.120 0.080 0.175	0.880 0.885 0.898 0.913 1.105 1.144 LOSS P TOT 0.062 0.059 0.038 0.028	1.571 1.563 1.550 1.548 1.277 1.217 ARAM PROF 0.051 0.045 0.045 0.016 0.033
7 8 9 10 11 RP 1 2 3 4 5 6	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT 5PAN 7.00 11.70 30.90 40.40 42.80 45.20	0.677 0.690 0.710 0.726 0.747 0.768 0.793 INCI MEAN 8.8 8.2 7.0 4.2 6.1	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6 3.1 -0.1 1.6 1.5	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6 3.8	0.598 0.602 0.606 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.438 0.472 0.477	0.485 0.492 0.502 0.513 0.555 0.560 0.560 EFF 0.402 0.509 0.783 0.848 0.751 0.757	TOT 0.599 0.450 0.201 0.142 0.238 0.237	PROF 0.485 0.343 0.120 0.080 0.175 0.177	0.880 0.885 0.898 0.913 0.913 1.105 1.144 LOSS P TOT 0.062 0.059 0.038 0.046 0.046	1.571 1.563 1.550 1.548 1.277 1.217 ARAM PROF 0.051 0.045 0.023 0.016 0.033 0.034
7 8 9 10 11 RP 1 2 3 4 5 6 7	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90	0.677 0.690 0.716 0.726 0.747 0.768 0.793 INCI MEAN 8.8 8.8 8.2 7.0 4.2 6.1 6.1	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.56 3.1 -0.1 1.6	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6 3.8 2.4	0.598 0.602 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.438 0.472 0.472	0.485 0.492 0.502 0.513 0.555 0.560 0.560 EFF 0.402 0.793 0.848 0.757 0.770	TOT 0.599 0.450 0.201 0.142 0.238 0.237 0.231	PROF 0.485 0.343 0.120 0.080 0.175 0.177 0.174	0.880 0.885 0.895 0.995 1.105 1.144 LOSS P TOT 0.062 0.059 0.038 0.028 0.046 0.046	1.571 1.563 1.554 1.548 1.483 1.277 1.217 ARAM PROF 0.051 0.045 0.023 0.016 0.033 0.034
7 8 9 10 11 RP 1 2 3 4 5 6 7 8	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN 7.00 11.70 30.90 42.80 42.80 45.20 45.20 50.00	0.677 0.690 0.716 0.747 0.768 0.793 INCI MEAN 8.8 8.2 7.2 6.1 6.1 6.1	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6 3.1 -0.1 1.6 1.5	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6 3.8 2.4 1.3	0.598 0.602 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.438 0.472 0.477 0.489	0.485 0.492 0.503 0.555 0.560 0.560 0.560 EFF 0.402 0.509 0.783 0.848 0.751 0.770 0.783	TOT 0.599 0.450 0.201 0.142 0.238 0.237 0.231	PROF 0.485 0.343 0.120 0.080 0.175 0.177 0.174 0.168	0.880 0.885 0.898 0.995 1.105 1.144 LOSS TOT 0.062 0.038 0.028 0.046 0.046 0.046	1.571 1.563 1.554 1.548 1.483 1.277 1.217 ARAM PROF 0.051 0.045 0.045 0.033 0.034
7 8 9 10 11 RP 1 2 3 4 5 6 7	0.598 0.603 0.606 0.608 0.593 0.533 0.514 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90	0.677 0.690 0.716 0.726 0.747 0.768 0.793 INCI MEAN 8.8 8.8 8.2 7.0 4.2 6.1 6.1	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6 3.1 -0.1 1.6 1.4 1.4	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6 3.8 2.4	0.598 0.602 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.438 0.472 0.472	0.485 0.492 0.502 0.513 0.555 0.560 0.560 EFF 0.402 0.793 0.848 0.757 0.770	TOT 0.599 0.450 0.201 0.142 0.238 0.237 0.231	PROF 0.485 0.343 0.120 0.080 0.175 0.177 0.174	0.880 0.885 0.898 0.913 1.105 1.144 LOSS P TOT 0.062 0.059 0.038 0.028 0.046 0.046 0.046 0.045 0.045	1.571 1.563 1.558 1.548 1.277 1.217 ARAM PROF 0.051 0.045 0.033 0.034 0.034 0.035 0.034 0.014
7 8 9 10 11 RP 12 3 4 5 6 7 8 9	0.598 0.603 0.606 0.698 0.593 0.514 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 47.90 50.00 71.80	0.677 0.690 0.716 0.747 0.768 0.793 INC MEAN 8.8 8.2 7.0 6.1 6.1 6.1 6.2 7.3	1.188 1.180 1.167 1.161 1.032 0.895 0.852 IDENCE SS 6.5 5.6 3.1 -0.1 1.6 1.5	0.700 0.689 0.677 0.673 0.662 0.617 0.596 DEV 22.6 17.5 5.0 2.8 4.6 3.8 2.4 1.3 3.9	0.598 0.602 0.608 0.593 0.532 0.514 D-FACT 0.460 0.421 0.477 0.485 0.472 0.498 0.436	0.485 0.492 0.502 0.513 0.555 0.560 0.560 EFF 0.402 0.793 0.783 0.751 0.757 0.770 0.783	TOT 0.599 0.450 0.201 0.142 0.238 0.237 0.231 0.223	PROF 0.485 0.343 0.120 0.080 0.175 0.177 0.174 0.168 0.072	0.880 0.885 0.898 0.995 1.105 1.144 LOSS P. TOT 0.062 0.058 0.028 0.046 0.046 0.046 0.046	1.571 1.563 1.558 1.548 1.483 1.277 1.217 ARAM PROF 0.051 0.023 0.016 0.033 0.034 0.034 0.034

TABLE VII. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES FOR DEEP,

LONG BLADE-ANGLE SLOT CASING

(e) Reading number, 555-1106

RP 1 2 3 4 5 6 7 8 9	RP 1 2 3 4 5 6 7 8 9 1 0 1 1	RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11
PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	ABS M 1N 0.387 0.418 0.500 0.541 0.555 0.5559 0.559 0.559 0.555 0.489	ABS IN 427.2 459.4 545.1 587.1 598.0 602.0 604.4 605.1 603.3 548.8 532.2	9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377
INC MEAN 10.7 9.9 8.1 7.8 7.9 8.1 8.2 8.8	ACH NO 0.468 0.496 0.659 0.677 0.678 0.691 0.711 0.725 0.744 0.772 0.799	VEL 0UT 589.9 615.8 774.0 791.1 792.9 807.8 829.9 845.2 853.3 880.7 910.3	9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201
DENCE SS 8.4 7.4 5.1 3.8 3.4 3.4 3.4 2.9 3.5 3.5	REL M 1N 1.262 1.248 1.190 1.164 1.159 1.152 1.143 1.008 0.875 0.834	REL IN 1392.2 1372.1 1298.0 1262.7 1255.7 1247.2 1236.2 1222.9 1091.3 951.8 908.6	IN 3.3 3.6 2.9 2.5 2.0 1.6 1.5 1.7
DEV 26.8 20.6 5.3 4.5 4.6 3.7 21.2 3.7 5.2 3.3	ACH NO 0.640 0.669 0.736 0.714 0.693 0.683 0.671 0.665 0.652 0.614 0.591	VEL 0UT 807.0 830.0 864.8 834.5 809.8 798.2 782.3 774.4 748.0 700.6 673.6	0UT 70.2 60.8 44.9 45.1 45.5 45.6 42.6 43.6
D-FACT 0.544 0.513 0.450 0.455 0.474 0.481 0.495 0.495 0.435 0.391 0.395	MERID M 10 0.387 0.417 0.499 0.541 0.552 0.556 0.559 0.559 0.559 0.559	MERI 1N 426.6 458.5 544.4 5586.5 597.5 601.6 604.1 604.9 603.1 548.6 531.9	IN 72.2 70.5 65.2 62.3 61.6 61.7 60.4 56.5 54.8
0.347 0.392 0.760 0.773 0.748 0.750 0.763 0.779 0.910 0.931	OLT 0.159 0.159 0.242 0.470 0.489 0.488 0.498 0.508 0.508 0.548 0.559	D VEL 0UT 200.1 300.1 552.0 571.2 561.8 570.2 581.3 591.6 628.2 638.9 637.4	OUT 75.6 68.8 50.3 46.8 46.1 44.4 42.0 40.2 32.9 24.2 18.9
LOSS C TOT 0.727 0.650 0.229 0.221 0.250 0.253 0.248 0.236 0.101 0.096 0.136		TAN IN 24.2 29.1 27.3 25.2 23.5 20.4 16.9 16.0	1N 521.5 520.4 520.0 518.6 517.6 517.6 517.6 517.9 517.5
OEFF PROF 0.602 0.534 0.159 0.183 0.188 0.185 0.177 0.069 0.095 0.136		6 VEL 0UT 554.9 537.7 542.6 547.3 559.5 572.2 592.3 603.6 577.5 606.1 650.0	RATIO 1.325 1.291 1.200 1.196 1.200 1.203 1.206 1.207 1.173 1.170
LOSS P TOT 0.059 0.075 0.043 0.042 0.048 0.049 0.049 0.019 0.017		WHEEL IN 1349.5 1322.3 1205.5 1143.4 1127.9 1113.0 1094.9 1079.7 925.5 794.8 752.6	IN 14.51 14.65 14.68 14.71 14.72 14.72 14.72 14.73 14.73
ARAM PROF 0.049 0.062 0.029 0.035 0.037 0.037 0.036 0.013	PEAK SSMACH NO 1.781 1.786 1.690 1.622 1.609 1.604 1.591 1.528	1311.5 1208.3 1155.6 1142.8 1130.9 1115.8	RAT10 1.453 1.460 1.641 1.639 1.628 1.642 1.666 1.666 1.670 1.675

TABLE VIII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW, LONG

(a) Reading number, 707-1503

	DV	110	ARG	BETAM	REI	_ BETAM	TOTA	AL TEMP	TOTA	L PRESS
RP	IN	OUT	IN	0UT	IN	OUT	IN	RAT [0 1.360	IN 14.53	RATIO
1 2	9.622 9.426	9.531 9.349	1.5 2.3	73.3 64.1	70.5	72.9 64.1	521.1 521.1	1.339	14.55	
3	8.587 8.152	8.607 8.239	1.2	48.3 47.4	65.5 62.7	49.8 45.8	519.9 519.0	1.205	14.69	
5	8.040	8.146	0.9	48.1	62.0	45.2	518.9	1.202	14.72	1.637
6 7	7.927 7.800	8.054 7.949	0.8 0.1	48.3 48.5	61.4 61.1	43.5 41.2	518.2 516.8	1.203	14.72	
8	7.700	7.868	0.3	48.3	60.6	39.4	517.9	1.207	14.72	1.690
9 10	6.611 5.681	7.025 6.387	-0.0 0.1	45.5 46.3	56.7 54.9	31.2 21.8	517.1 517.8	1.176	14.72	
11	5.377	6.201	-0.2	47.7	55.0	16.3	517.2	1.180	14.73	
	ABS	VEL	REL	VEL	MERI	D VEL	TAN	IG VEL	WHEE	L SPEED
RP 1	IN 434.6	0UT 704.6	IN 1403.3	0UT 689.0	[N 434,4	0UT 203.0	IN 11.6	0UT 674.7	IN	0UT 1333.2
2	460.2	728.2	1380.0	727.0	459.8	318.0	18.5	655.0		1308.8
3 4	543.9 584.0	786.3 804.6	1309.7 1271.3	809.4 781.3	543.8 584.0	522.7 545.0	11.1	587.4 591.9		1205.3
5	594.7	806.2	1266.0	762.8	594.7	537.9	8.9	600.6	1126.5	1141,4
6 7	600.4 600.2	817.7 835.7	1254.3 1242.7	749.7 736.3	600.3 600.2	543.6 554.1	8.0 1.5	610.9 625.6		1127.1
8	605.8	852.2	1234.7	734.3	605.8	567.3	2.7	635.9	1078.6	1102.1
9 10	609.1 556.4	865.2 893.8	1108.5 968.8	708.1 665.5	609.1 556.4	606.0 618.0	-0.3 1.1	617.5 645.8	925.9 794.2	983.9 892.9
11	529.0	926.7	921.2	650.2	529.0	624.1	-2.1	685.0	752.1	867.4
		ACH NO			MERID M				MERID	PEAK SS
RP !	IN 0.394	0UT 0.556	IN 1.273	0UT 0.544	IN 0.394	0UT 0.160			VEL R	MACH NO 1.785
2	0.418	0.581	1.255	0.580	0.418	0.254			0.692	1.764
3 4	0.499 0.538	0.669 0.688	1.201 1.171	0.689 0.669	0.498 0.538	0.445 0.466			0.961 0.933	1.708 1.639
5	0.548 0.554	0.689 0.700	1.167 1.158	0.652 0.642	0.548 0.554	0.460 0.465			0.905	1.628 1.617
6 7	0.555	0.717	1,149	0.632	0.555	0.476			0.923	1.617
8 9	0.560 0.564	0.732 0.755	1.141	0.630 0.618	0.560 0.564	0.487 0.529			0.936 0.995	1.607 1.539
10	0.512	0.786	0.891	0.585	0.512	0.543			1.111	1.318
11	0.486	0.814	0.846	0.571	0.486	0.548			1.180	1.268
	PERCENT		DENCE	DEV	D-FACT	EFF	LOSS C		LOSS P	
RP 1	SPAN 7.00	MEAN 10.5	SS 8.2	24.1	0.663	0.364	TOT 0.749	PROF 0.621	TOT 0.072	PROF 0.060
2	11.70	10.0	7,4	15.8	0.620	0.400	0.703	0.584	0.098	0.082
3 4	30.90 40.40	9.2 8.4	5.4 4.1	4.8 3.5	0.511 0.514	0.744	0.246 0.225	0.150 0.150	0.047	0.028 0.029
5 6	42.80	8.2	3.8	3.6	0.527	0.749	0.250	0.177 0.179	0.049	0.034
7	45.20 47.90	8.2 8.5	3.6 3.8	2.8 1.5	0.534 0.543	0.755 0.764	0.248 0.244	0.177	0.049 0.049	0.035 0.036
8 9	50.00 71.80	8.4 9.0	3.6 3.1	0.5 2.0	0.543	0.780 0.905	0.233	0.169 0.069	0.048	0.035 0.014
10	88.30	10.2	3.7	2.8	0.449	0.947	0.072	0.069	0.013	0.012
11	93.10	11.0	4.3	0.8	0.439	0.923	0.120	0.120	0.021	0.021

TABLE VIII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

(b) Reading number, 708-1514

RP 1 23345 6789 1011	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.946 7.868 7.025 6.387 6.201	ABS IN 0.4 0.9 1.0 0.7 0.5 0.6 0.4 0.4	BETAM OUT 54.5 43.6 41.8 42.6 43.6 44.2 44.8 44.4 41.4 43.5 45.2	REL IN 67.7 66.2 60.6 57.8 57.0 56.5 52.3 55.8 53.0 51.9	BETAM OUT 63.2 58.0 49.1 46.8 46.4 44.7 39.9 40.6 32.5 23.3 17.5	TOTAL IN 520.7 519.8 519.3 518.6 518.6 518.9 518.4 517.7 517.7	TEMP RATIO 1.269 1.195 1.185 1.179 1.180 1.182 1.186 1.158 1.150 1.170	TOTAL IN 14.51 14.62 14.71 14.72 14.73 14.75 14.72 14.73 14.73	PRESS RATIO 1.477 1.527 1.590 1.555 1.538 1.648 1.644 1.627 1.658
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 550.0 577.1 670.9 712.5 727.3 727.2 838.7 727.2 692.2 621.8 602.0	VEL 0UT 679.8 707.8 788.9 788.1 786.1 800.5 856.7 838.9 861.8 892.9 931.1	REL IN 1451.4 1431.5 1366.0 1336.5 1334.7 1319.0 1371.9 1294.9 1150.9 1008.7 960.3	VEL OUT 875.1 967.0 897.7 848.3 824.7 806.7 792.2 788.7 766.7 704.5 688.1	MERI IN 550.0 577.1 670.8 712.5 727.3 727.2 838.7 727.2 622.3 602.0	D VEL OUT 394.8 512.3 587.8 580.5 568.9 573.7 607.7 599.2 646.4 647.2 656.1	TAN(IN 4.0 9.4 11.9 8.7 7.3 5.5 5.2 4.9 0.4 4.6	G VEL OUT 553.4 488.4 526.1 533.1 542.5 558.3 603.9 587.2 570.0 615.2 660.7	WHEEL IN 1347.2 1319.4 1201.8 1139.5 1124.9 1107.7 1091.2 1076.6 924.4 794.7 752.8	1308.6 1204.6 1151.6 1139.7 1125.4 1112.1 1100.1 982.3 893.5
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.504 0.531 0.624 0.681 0.681 0.797 0.681 0.576 0.576	ACH NO OUT 0.556 0.600 0.678 0.680 0.677 0.690 0.742 0.726 0.758 0.792 0.822	REL M 1.330 1.317 1.270 1.249 1.250 1.235 1.304 1.213 1.074 0.987	ACH NO OUT 0.716 0.820 0.772 0.732 0.711 0.696 0.687 0.682 0.625 0.625	MERID M IN 0.504 0.531 0.623 0.666 0.681 0.797 0.681 0.596 0.576	ACH NO OUT 0.323 0.434 0.505 0.490 0.495 0.527 0.518 0.569 0.579				PEAK SS MACH NO 1.694 1.674 1.603 1.541 1.529 1.516 1.452 1.503 1.439 1.283 1.213
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 6.27 4.3 5.5 3.2 3.3 -0.3 5.4 7.2	3.9 3.1 0.5 -0.8 -1.2 -1.2 -5.0 -1.2 -0.5	DEV 14.4 9.8 4.1 4.5 4.9 0.2 1.6 3.4 4.2	D-FACT 0.520 0.431 0.453 0.476 0.494 0.503 0.541 0.511 0.449 0.426 0.417	0.438 0.658 0.766 0.752 0.726 0.730 0.817 0.764 0.927 0.994 0.915	LOSS C TOT 0.540 0.278 0.196 0.207 0.230 0.232 0.154 0.213 0.070 0.007	0EFF PR0F 0.427 0.1172 0.114 0.166 0.172 0.097 0.160 0.043 0.003	LOSS F TOT 0.080 0.047 0.038 0.040 0.044 0.045 0.032 0.043 0.013	PARAM PROF 0.063 0.029 0.022 0.032 0.033 0.030 0.032 0.032 0.038 0.001

TABLE VIII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

(c) Reading number, 709-1525

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.868 7.025 6.387 6.201	ABS IN 1.3 1.6 0.5 0.6 0.4 0.5 0.4 0.1	BETAM 0UT 63.7 53.2 44.3 45.3 46.3 46.9 46.8 44.2 45.4	REI IN 68.1 67.1 59.7 58.9 58.4 55.0 57.4.5 53.1 52.5	BETAM 0UT 66.3 60.0 48.4 46.0 45.2 43.5 39.1 39.3 31.4 22.7 16.6	TOTA 1N 520.5 519.5 519.2 517.7 518.6 518.4 518.4 518.4 518.4	RAT [0 1.321 1.261 1.197 1.194 1.193 1.195 1.199 1.198 1.166 1.156	TOTAL PRESS IN RATIO 14.63 1.520 14.64 1.547 14.67 1.665 14.67 1.631 14.69 1.629 14.71 1.724 14.72 1.669 14.73 1.667 14.73 1.660 14.73 1.660
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 536.9 544.1 626.1 661.9 673.5 680.5 760.0 685.0 695.3 574.2	VEL 0UT 701.9 711.8 800.0 799.8 803.1 816.8 865.8 851.7 864.4 888.7 926.9	REL IN 1440.2 1415.8 1338.7 1312.7 1305.3 1296.9 1325.6 1270.7 1133.4 988.2 944.0	VEL OUT 771.9 852.9 862.3 171.1 788.2 774.2 763.1 753.7 726.7 676.3 658.7	MERI IN 536.8 544.0 625.8 661.9 673.5 680.5 70685.0 658.4 593.2 574.1	D VEL OUT 310.8 426.3 572.5 563.0 555.2 561.5 592.0 620.2 624.0 631.4	TAN IN 12.3 12.4 17.4 6.1 6.8 4.4 6.2 4.8 0.8 4.3	G VEL 0UT 629.4 570.0 558.8 568.0 580.3 593.2 631.7 620.9 602.2 632.7 678.5	WHEEL SPEED IN OUT 1348.7 1335.9 1319.5 1308.7 1200.8 1203.6 1139.7 1151.9 1124.9 1139.7 1108.4 1126.2 1092.4 1113.2 1075.1 1098.6 923.2 981.0 794.7 893.5 751.1 866.3
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M. IN 0.492 0.499 0.579 0.616 0.627 0.634 0.715 0.638 0.612 0.529	OUT 0.563 0.587 0.685 0.687 0.689 0.702 0.747 0.757 0.756 0.817	REL M. 1.319 1.298 1.221 1.214 1.208 1.247 1.184 1.053 0.912 0.869	OUT 0.619 0.703 0.738 0.696 0.665 0.665 0.649 0.649 0.637 0.598 0.598	MERID M IN 0.491 0.499 0.579 0.616 0.627 0.634 0.715 0.638 0.612 0.548 0.529	ACH NO OUT 0.249 0.351 0.490 0.483 0.477 0.482 0.502 0.502 0.552 0.557			MERID PEAK SS VEL R MACH NO 0.579 1.696 0.784 1.697 0.915 1.627 0.851 1.584 0.779 1.492 0.851 1.531 0.942 1.477 1.052 1.290 1.100 1.230
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 6.9 5.8 5.5 5.1 2.4 6.8 8.4 8.5	DENCE SS 4.3 2.0 1.2 0.8 0.6 -2.3 0.4 0.9 1.8 1.9	DEV 17.4 11.8 3.4 3.7 3.7 2.8 -0.6 0.4 2.3 3.7	D-FACT 0.603 0.523 0.475 0.502 0.518 0.528 0.552 0.537 0.483 0.446 0.442	EFF 0.395 0.509 0.797 0.774 0.764 0.768 0.847 0.797 0.934 1.001 0.947	LOSS CO TOT 0.649 0.484 0.185 0.207 0.217 0.218 0.199 0.068 -0.002	PROF 0.537 0.376 0.102 0.137 0.151 0.155 0.088 0.144 0.038	LOSS PARAM TOT PROF 0.085 0.071 0.078 0.060 0.036 0.027 0.042 0.029 0.043 0.031 0.030 0.018 0.041 0.030 0.013 0.007 -0.000 -0.001 0.013 0.013

TABLE VIII. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

(d) Reading number, 710-1536

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.946 7.968 7.025 6.387 6.201	ABS IN 1.4 1.1 1.2 0.7 0.6 0.5 0.4 0.2 0.3	BETAM OUT 67.0 66.7 45.6 46.5 47.2 47.4 47.5 47.4 45.2 45.9	RELL IN 68.8 68.1 63.2 60.7 59.8 59.3 58.6 55.4 53.9 53.4	BETAM 0UT 68.7 61.5 48.5 45.7 44.8 43.0 40.8 38.9 31.1 23.1 16.3	TOTAL TEMP IN RATIO 520.9 1.332 520.3 1.284 519.5 1.201 518.2 1.198 518.0 1.200 518.3 1.202 517.7 1.204 517.6 1.163 517.8 1.145 518.3 1.169	TOTAL PRESS IN RATIO 14.66 1.525 14.66 1.550 14.67 1.678 14.69 1.654 14.70 1.654 14.71 1.656 14.71 1.674 14.70 1.701 14.71 1.682 14.73 1.679 14.73 1.699
RP 1 2 3 4 5 6 7 8 9 10	ABS 1N 518.0 524.9 600.3 635.9 648.5 654.6 657.1 657.1 636.3 576.9 555.6	VEL 0UT 693.4 706.6 799.3 805.1 807.1 822.1 841.1 857.8 865.9 880.1 922.6	REL IN 1429.8 1407.8 1329.6 1298.1 1289.8 1281.2 1269.4 1259.8 1119.7 979.3 932.7	VEL OUT 745.6 813.7 842.6 793.1 772.6 761.8 750.5 746.5 712.7 666.1 645.0	MERI IN 517.9 524.8 600.2 635.9 648.5 657.1 657.1 636.3 576.9 555.6	D VEL OUT 271.1 388.4 558.8 554.2 548.1 5567.9 567.9 567.9 610.2 612.9 619.0	TANG VEL IN OUT 12.9 638.2 9.7 590.4 13.0 571.6 7.4 584.0 7.2 592.4 5.4 604.7 4.3 620.5 2.3 631.4 3.4 614.4 2.4 631.6 1.4 684.2	HHEEL SPEED IN OUT 1345.6 1332.8 1316.1 1305.4 1199.4 1202.2 1139.1 1151.3 1122.2 1137.0 1106.8 1124.5 1090.3 1111.2 1077.1 1100.6 924.7 982.7 793.8 892.5 750.6 865.6
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M. IN 0.473 0.480 0.554 0.589 0.608 0.611 0.592 0.511	ACH NO OUT 0.553 0.576 0.683 0.690 0.692 0.705 0.722 0.738 0.760 0.781	REL M. 1.306 1.288 1.226 1.203 1.197 1.190 1.179 1.171 1.038 0.902 0.857	ACH NO OUT 0.595 0.663 0.720 0.662 0.662 0.654 0.645 0.645 0.645 0.569	MERID M IN 0.473 0.480 0.553 0.589 0.602 0.608 0.610 0.511 0.590 0.532	ACH NO OUT 0.216 0.317 0.477 0.475 0.478 0.478 0.488 0.500 0.536 0.544		MERID PEAK SS VEL R MACH NO 0.523 1.706 0.740 1.711 0.931 1.651 0.872 1.598 0.845 1.579 0.851 1.579 0.864 1.563 0.884 1.563 0.884 1.560 0.959 1.500 1.062 1.302 1.114 1.241
RP 1 2 3 4 5 6 7 8 9	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 7.3 7.6 6.9 6.4 6.1 6.1 6.2 7.7 9.2	5.0 5.0 3.1 2.1 1.6 1.5 1.6 1.8	DEV 19.9 13.3 3.4 3.4 3.5 2.5 1.1 -0.0 2.0 4.0 0.8	D-FACT 0.621 0.554 0.490 0.514 0.527 0.534 0.541 0.541 0.492 0.451	0.386 0.470 0.794 0.788 0.768 0.765 0.785 0.803 0.980 1.088 0.970	LOSS COEFF TOT PROF 0.676 0.563 0.551 0.441 0.192 0.106 0.201 0.130 0.222 0.156 0.218 0.154 0.214 0.154 0.201 0.142 0.020 -0.011 -0.105 -0.108 0.043 0.043	LOSS PARAM TOT PROF 0.080 0.067 0.084 0.067 0.037 0.021 0.039 0.025 0.043 0.030 0.044 0.031 0.044 0.031 0.044 -0.002 -0.019 -0.019 0.007 0.007

TABLE VIII. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

(e) Reading number, 711-1547

RP 1 2 3 4 5 6 7 8 9 10 11	RAE IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.377	011 9.531 9.349 8.607 8.239 8.146 8.054 7.968 7.025 6.387 6.201	ABS IN 1.6 1.5 1.1 0.7 0.5 0.6 0.5 0.4 0.0	BETAM OUT 72.2 63.2 48.2 47.8 48.4 48.6 48.5 45.5 45.5	REL IN 71.4 70.8 66.0 63.3 62.6 62.1 61.2 57.4 55.8	BETAM 0UT 72.0 63.6 49.8 45.8 45.0 43.4 41.5 39.2 31.5 21.7 16.3	IN 521.7 521.1 520.0 518.7 517.9 517.6 517.2 517.5 517.2	TEMP RATIO 1.356 1.353 1.206 1.201 1.205 1.204 1.206 1.207 1.172 1.165 1.179	TOTAL IN 14.64 14.64 14.66 14.69 14.70 14.72 14.71 14.73 14.73	PRESS RATIO 1.547 1.575 1.657 1.664 1.652 1.658 1.679 1.679 1.679
RP 1 2 3 4 5 6 7 8 9 10 11	ABS IN 446.8 454.8 530.3 568.3 582.6 587.4 588.0 589.9 539.4 518.7	703.3 725.0 783.6 804.4 806.2 816.8 851.9 851.9 858.8 892.2 923.0	REL IN 1402.3 1381.2 1303.1 1266.9 1259.0 1244.7 1233.5 1221.6 1095.3 960.1 911.5	VEL OUT 693.5 734.8 810.2 775.0 757.2 741.0 733.9 729.1 705.1 661.5 645.1	MERI IN 446.7 454.6 530.2 568.5 579.2 582.6 587.4 588.0 589.9 539.4 518.7	D VEL OUT 214.8 327.1 522.7 540.5 538.1 549.9 565.0 601.4 614.4 619.2	IN 12.5 11.5 9.8 6.8 5.4 6.1 4.0 0.5	VEL 0UT 669.7 647.0 583.9 595.7 602.7 614.4 624.2 637.5 613.1 647.0 684.4	WHEEL IN 1341.8 1315.7 1200.1 1138.9 1123.2 1106.1 1089.3 1074.9 923.4 793.4 750.3	1305.0 1202.9 1151.1 1138.0 1123.8 1110.2
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.406 0.413 0.485 0.523 0.534 0.537 0.542 0.543 0.545 0.475	0.556 0.580 0.666 0.688 0.689 0.699 0.713 0.751 0.751 0.786	REL M IN 1.273 1.255 1.193 1.165 1.160 1.148 1.139 1.127 1.011 0.882 0.835	ACH NO OUT 0.548 0.587 0.663 0.663 0.648 0.629 0.626 0.616 0.583 0.566	MERID M IN 0.405 0.413 0.485 0.523 0.534 0.534 0.542 0.542 0.545 0.475	ACH NO OUT 0.170 0.262 0.444 0.462 0.458 0.461 0.471 0.485 0.526 0.541				PEAK SS MACH NO 1.766 1.772 1.719 1.658 1.644 1.632 1.624 1.618 1.560 1.331
RP 1 2 3 4 5 6 7 8 9	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 9.9 10.2 9.7 9.1 8.9 8.9 9.0 9.8 11.1	DENCE SS 7.6 7.7 5.9 4.8 4.4 4.3 4.2 4.2 3.9 4.5	DEV 23.2 15.4 4.8 3.5 2.7 1.8 0.3 2.3 0.8	D-FACT 0.658 0.615 0.508 0.519 0.530 0.539 0.541 0.542 0.447 0.438	0.373 0.416 0.755 0.779 0.759 0.762 0.769 0.793 0.929 0.988 0.926	0.735 (0.680 (0.238 (0.219 (0.243 (0.244 (0.242 (0.222 (0.079 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.016 (0.	EFF PROF 0.613 0.559 0.141 0.141 0.168 0.174 0.175 0.157 0.041	LOSS P TOT 0.074 0.097 0.045 0.043 0.047 0.048 0.049 0.046 0.015 0.003	PROF 0.062 0.080 0.027 0.027 0.033 0.034 0.035 0.032 0.000 0.002

TABLE IX. - BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW, SHORT

(a) Reading number, 761-1629

				J		-				
	RAD	11	ABS	BETAM	REL	BETAM	TOTA	L TEMP	TOTAL	PRESS
RP	IN	OUT	IN	OUT	IN	OUT	IN	RATIO	IN	RAT10
1	9.622	9.531	0.7	64.7	70.3	56.7	520.0	1.353	14.52	2.050
ż	9.426	9.349	1.1	60.2	68.9	54.5	519.8	1.309	14.64	2.011
7						48.3	519.1	1.251	14.72	1.934
3	8.587	8.607	0.6	54.7	64.6					
4	8.152	8.239	0.3	55.8	62.6	46.1	518.3	1.245	14.72	1.889
5 6	B.040	8.146	0.3	56.1	62.0	45.5	518.2	1.243	14.73	1.874
6	7.927	8.054	0.3	56.0	61.7	44.6	519.0	1.236	14.73	1.862
7	7.800	7.949	0.2	55.4	61.3	43.3	518.0	1.232	14.72	1.863
8	7.700	7.868	0.1	54.8	61.0	42.7	518.1	1.227	14.73	1.855
9	6.611	7.025	-0.1	54.1	57.9	36.0	518.1	1.193	14,72	1.736
10	5.681	6.387	0.2	51.7	55.7	25.6	518.4	1.178	14.72	1.729
11	5.377	6.201	0.1	52.5	55.4	19.8	518.3	1.182	14.70	1.751
	ABS	VEL	REL	٧EL	MERI	D √EL	TAN	G VEL	WHEEL	SPEED
RP	[N	OUT	(N	OUT	IN	OUT	IN	OUT	IN	OUT
1	479.9	856.2	1421.0	665.8	479.9	365.9	5.5	774.1	1343.0	
2	505.1	834.4	1400.5	714.3	505.0	415.0	9.7	723.9	1316.0	
3	564.4	819.1	1317.8	711.8	564.3	473.7	5.9	668.2	1196.7	
4	587.3	815.2	1278.3	660.7	587.3	458.2	2.8	674.2	1138.2	
=	593.7	813.5	1266.2	647.9	593.7	454.3	3.6	674.9	1122.0	
5 6	593.7	812.6	1251.1	638.2	593.9	454.3	3.2	673.7	1104.3	
5								673.7		
7	594.5	816.6	1237.5	636.2	594.5	463.3	2.4	672.5	1087.8	
8	594.4	813.8	1227.3	639.0	594.4	469.3	1.3	664.8	1075.0	
9	579.8	793.2	1090.5	575.1	579.8	465.5	-1.4	642.3	922.2	980.0
10	539.1	824.1	957.6	566.7	539.1	511.1	1.4	646.5	792.8	B91.4
11	517.3	854.2	910.5	552.2	517.3	519.5	1.2	678.1	750.5	865.5
		ACH NO			MERID M					PEAK SS
RP	IN	OUT	IN	OUT	IN_	OUT_			VEL R	MACH NO
1	0.437	0.689	1.295	0.536	0.437	0.295			0.763	1.747
2	0.462	0.682	1.280	0.584	0.461	0.339			0.822	1.729
3	0.519	0.686	1,211	0.596	0.519	0.397			0.839	1.689
4	0.541	0.685	1,179	0.555	0.541	0.385			0.780	1.645
5	0.548	0.684	1.168	0.545	0.548	0.382				1.631
5 6 7	0.548	0.685			0.500	U. 30Z			0.765	ינסיי
7		U.000	1.154	0.538	0.548	0.383			0.765 0.765	1.622
	0.549		1,154							
	0.549 0.549	0.690	1,142	0.538	0.548 0.549	0.383 0.391			0.765	1.622
8	0.549	0.690 0.689	1,142	0.538 0.541	0.548 0.549 0.549	0.383 0.391 0.397			0.765 0.779 0.790	1.622 1.618 1.615
8 9	0.549 0.534	0.690 0.689 0.680	1.142 1.133 1.005	0.538 0.541 0.493	0.548 0.549 0.549 0.534	0.383 0.391 0.397 0.399			0.765 0.779 0.790 0.803	1.622 1.618 1.615 1.575
8 9 10	0.549 0.534 0.495	0.690 0.689 0.680 0.714	1.142 1.133 1.005 0.879	0.538 0.541 0.493 0.491	0.548 0.549 0.549 0.534 0.495	0.383 0.391 0.397 0.399 0.443			0.765 0.779 0.790 0.803 0.948	1.622 1.618 1.615 1.575 1.324
8 9	0.549 0.534	0.690 0.689 0.680	1.142 1.133 1.005	0.538 0.541 0.493	0.548 0.549 0.549 0.534	0.383 0.391 0.397 0.399			0.765 0.779 0.790 0.803	1.622 1.618 1.615 1.575
8 9 10	0.549 0.534 0.495	0.690 0.689 0.680 0.714	1.142 1.133 1.005 0.879	0.538 0.541 0.493 0.491	0.548 0.549 0.549 0.534 0.495	0.383 0.391 0.397 0.399 0.443			0.765 0.779 0.790 0.803 0.948	1.622 1.618 1.615 1.575 1.324
8 9 10	0.549 0.534 0.495 0.474	0.690 0.689 0.680 0.714 0.742	1.142 1.133 1.005 0.879 0.834	0.538 0.541 0.493 0.491 0.480	0.548 0.549 0.549 0.534 0.495 0.474	0.383 0.391 0.397 0.399 0.443 0.451	1055 (OFFF	0.765 0.779 0.790 0.803 0.948 1.004	1.622 1.618 1.615 1.575 1.324 1.263
9 10 11	0.549 0.534 0.495 0.474 PERCENT	0.690 0.689 0.680 0.714 0.742	1.142 1.133 1.005 0.879 0.834	0.538 0.541 0.493 0.491	0.548 0.549 0.549 0.534 0.495	0.383 0.391 0.397 0.399 0.443 0.451	LOSS C		0.765 0.779 0.790 0.803 0.948 1.004	1.622 1.618 1.615 1.575 1.324 1.263
8 9 10 11	0.549 0.534 0.495 0.474 PERCENT SPAN	0.690 0.689 0.680 0.714 0.742 INC MEAN	1.142 1.133 1.005 0.879 0.834 IDENCE SS	0.538 0.541 0.493 0.491 0.480	0.548 0.549 0.549 0.534 0.495 0.474	0.383 0.391 0.397 0.399 0.443 0.451	TOT	PROF	0.765 0.779 0.790 0.803 0.948 1.004	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF
8 9 10 11	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5	0.538 0.541 0.493 0.491 0.480 DEV 7.8	0.548 0.549 0.549 0.534 0.495 0.474 D-FACT	0.383 0.391 0.397 0.399 0.443 0.451 EFF	TOT 0.445	PROF 0.324	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058
8 9 10 11 RP 1 2	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3	0.548 0.549 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653	0.383 0.391 0.397 0.399 0.443 0.451 EFF 0.646 0.714	TOT 0.445 0.340	PROF 0.324 0.227	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042
8 9 10 11 RP 1 2	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8 8.3 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3 3.3	0.548 0.549 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.608	0.383 0.391 0.397 0.399 0.443 0.451 EFF 0.646 0.714 0.826	TOT 0.445 0.340 0.197	PROF 0.324 0.227 0.104	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.039	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.020
B 9 10 11 RP 1 2 3	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8 8.3 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3 3.3 3.8	0.548 0.549 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.608 0.631	0.383 0.391 0.397 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813	TOT 0.445 0.340 0.197 0.216	PROF 0.324 0.227 0.104 0.138	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.063	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.020 0.027
B 9 10 11 RP 1 2 3	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8 8.3 8.3 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0	0.548 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.638 0.631	0.383 0.391 0.397 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813 0.809	TOT 0.445 0.340 0.197 0.216 0.222	PROF 0.324 0.227 0.104 0.138 0.149	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.039 0.042 0.042	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.027 0.029
8 9 10 11 RP 1 2 3 4 5 6	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20	0.690 0.689 0.680 0.714 0.742 INC MEAN 8.8 8.3 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 3.9	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.9	0.548 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.608 0.636 0.637	0.383 0.391 0.397 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813 0.809	TOT 0.445 0.340 0.197 0.216 0.222 0.205	PROF 0.324 0.227 0.104 0.138 0.149 0.136	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.039 0.042 0.043	1.622 1.618 1.615 1.575 1.524 1.263 ARAM PROF 0.058 0.042 0.020 0.027 0.029
8 9 10 11 RP 1 2 3 4 5 6 7	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90	0.690 0.689 0.714 0.742 INC MEAN 8.3 8.3 8.4 8.3 8.4	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9 3.9	0.538 0.541 0.493 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.5	0.548 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.608 0.631 0.635 0.637	0.383 0.391 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813 0.809 0.824	TOT 0.445 0.340 0.197 0.216 0.222 0.205 0.190	PROF 0.324 0.227 0.104 0.138 0.149 0.136 0.124	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.042 0.043 0.040 0.037	1.622 1.618 1.615 1.575 1.524 1.263 ARAM PROF 0.058 0.042 0.027 0.029 0.026 0.024
8 9 10 11 RP 1 2 3 4 5 6 7 8	0.549 0.534 0.495 0.474 PERCENT 5PAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00	0.690 0.689 0.714 0.742 INC MEAN 8.8 8.3 8.3 8.4 8.3	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9 4.0	0.538 0.541 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.9 3.5 3.8	0.548 0.549 0.534 0.534 0.474 D-FACT 0.707 0.653 0.608 0.631 0.636 0.633	0.383 0.391 0.399 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813 0.809 0.824 0.837 0.852	TOT 0.445 0.340 0.197 0.216 0.222 0.205 0.190 0.173	PROF 0.324 0.227 0.104 0.138 0.149 0.136 0.124 0.108	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.039 0.042 0.043 0.037	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.027 0.029 0.024 0.024
8 9 10 11 RP 1 2 3 4 5 6 7 8 9	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80	0.690 0.689 0.689 0.714 0.742 INC MEAN 8.8 8.3 8.4 8.3 8.4 8.7 8.8	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9 3.9 4.0 4.0	0.538 0.541 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.9 3.5 6.8	0.548 0.549 0.554 0.455 0.474 D-FACT 0.707 0.658 0.631 0.636 0.637 0.638	0.383 0.391 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.809 0.824 0.837 0.852 0.883	10T 0.445 0.340 0.197 0.216 0.222 0.205 0.190 0.173 0.144	PROF 0.324 0.227 0.104 0.138 0.149 0.136 0.124 0.108 0.104	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.034 0.045 0.047 0.037	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.027 0.029 0.026 0.024 0.024 0.019
8 9 10 11 RP 1 2 3 4 5 6 7 8 9 10	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30	0.690 0.689 0.714 0.742 INC MEAN 8.8 8.3 8.3 8.4 8.7 8.8 10.2	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9 4.0 4.0 4.3	0.538 0.541 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.9 3.5 3.8 6.5	0.548 0.549 0.534 0.495 0.474 D-FACT 0.707 0.653 0.608 0.631 0.633 0.624 0.611	0.383 0.391 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.813 0.809 0.824 0.837 0.852	10T 0.445 0.340 0.197 0.216 0.222 0.205 0.190 0.173 0.144 0.070	PROF 0.324 0.227 0.104 0.138 0.149 0.136 0.124 0.108 0.104 0.067	0.765 0.779 0.779 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.039 0.042 0.042 0.037 0.034	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.020 0.027 0.026 0.024 0.021 0.012
8 9 10 11 RP 1 2 3 4 5 6 7 8 9	0.549 0.534 0.495 0.474 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80	0.690 0.689 0.689 0.714 0.742 INC MEAN 8.8 8.3 8.4 8.3 8.4 8.7 8.8	1.142 1.133 1.005 0.879 0.834 IDENCE SS 6.5 5.7 4.5 4.1 3.9 3.9 4.0 4.0	0.538 0.541 0.491 0.480 DEV 7.8 6.3 3.3 3.8 4.0 3.9 3.5 6.8	0.548 0.549 0.554 0.455 0.474 D-FACT 0.707 0.658 0.631 0.636 0.637 0.638	0.383 0.391 0.399 0.443 0.451 EFF 0.646 0.714 0.826 0.809 0.824 0.837 0.852 0.883	10T 0.445 0.340 0.197 0.216 0.222 0.205 0.190 0.173 0.144	PROF 0.324 0.227 0.104 0.138 0.149 0.136 0.124 0.108 0.104	0.765 0.779 0.790 0.803 0.948 1.004 LOSS P TOT 0.080 0.063 0.034 0.045 0.047 0.037	1.622 1.618 1.615 1.575 1.324 1.263 ARAM PROF 0.058 0.042 0.027 0.029 0.026 0.024 0.024 0.019

TABLE IX. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

SHORT BLADE-ANGLE SLOT CASING

(b) Reading number, 762-1640

	240		ADC	BETAM	DE1	BETAM	TOTA	AL TEMP	TATAL	_ PRESS
RP	RAD IN	OUT	IN	0UT	1N	OUT	IN	RATIO	IN	RATIO
1 2	9.622 9.426	9.531 9.349	1.0 0.7	53.0 47.4	66.2 64.4	55.8 54.1	520.1 519.1	1.282	14.46	1.854
2 3 4	8.587	8.607	0.4	46.7 48.2	59.5 57.0	46.9 46.1	518.5 519.0	1.224	14.72	1.839
5 6	8.152 8.040	8.239 8.146	0.2	48.7	56.4	46.1	518.4	1.209	14.73	1.738
6 7	7.927 7.800	8.054 7.949	0.4	48.7 47.9	56.0 55.3	45.8 44.4	518.4 519.0	1.203	14.72	1.722
8	7.700	7.868	0.2	47.1	55.2	43.2	518.8	1.195	14.72	1.733
9 10	6.611 5.681	7.025 6.387	0.1 0.2	45.8 46.7	52.7 50.8	35.2 25.7	518.1 518.3	1.170	14.72	1.673
11	5.377	6.201	0.2	47.9	50.3	20.4	518.6	1.175	14.71	1.689
		VEL		VEL		D VEL		G VEL		. SPEED
RP 1	IN 587.6	0UT 789.3	IN 1456.1	0UT 845.2	[N 587.5	0UT 475.0	IN 9.8	0UT 630.3	(N 1342.1	0UT 1329.4
2	627.7	781.9	1453.6	903.8	627.7	529.4	7.7	575.5	1318.7	1308.0
3	703.7 738.2	823.5 802.4	1388.2 1354.0	828.0 770.1	703.7 738.2	565.2 534.4	4.5 5.8	598.8 598.5	1201.1 1140.9	
5	745.0 745.6	793.7 787.4	1347.6 1331.8	755.1 745.8	745.0 745.6	524.0 520.0	2.0 4.6	596.1 591.3	1124.9 1108.1	
7	751.4	794.2	1321.0	745.5	751.4	532.3	4.1	589.4	1090.5	1111.3
8 9	745.9 702.5	800.4 811.2	1306.5 1158.4	747.4 692.1	745.9 702.5	544.5 565.8	2.5 0.9	586.6 581.2	1075.2	1098.6 979.7
10	644.6 622.0	844.0 874.5	1020.7 973.8	642.6 625.5	644.6 622.0	579.0 586.3	2.6 2.5	614.1	794.1 751.8	892.7 867.0
'''	022.V	614.5	313.0	025.5	022.V	300.3	2.5	040.3	751.6	007.0
		ACH NO			MERID M					PEAK SS
RP 1	IN 0.541	0UT 0.649	IN 1.340	0.695	IN 0.541	0UT 0.391			0.809	MACH NO 1.652
2 3	0.581 0.657	0.654 0.699	1.345 1.296	0.756 0.702	0.581 0.657	0.443			0.843 0.803	1.640
4	0.692	0.682	1.269	0.655	0.692	0.454			0.724	1.531
5 6	0.699 0.700	0.676 0.672	1.265 1.250	0.643 0.636	0.699 0.700	0.446 0.444			0.703 0.697	1.524
7 8	0.706 0.700	0.679 0.686	1.240	0.638 0.641	0.706 0.700	0.455			0.708 0.730	1.497
9	0.656	0.705	1.082	0.601	0.656	0.492			0.805	1.431
10 11	0.598 0.575	0.737 0.764	0.947 0.901	0.561 0.546	0.598 0.575	0.505 0.512			0.898 0.943	1.264
•••	V.515	4.104	4134		•••	11372			V.5-5	
RP	PERCENT SPAN	INC MEAN	IDENCE SS	DEV	D-FACT	EFF	LOSS C	OEFF PROF	LOSS P	ARAM PROF
1	7.00	4.7	2.4	7.0	0.558	0.683	0.334	0.230	0.061	0.042
2 3	11.70 30.90	3.9 3.2	1.3 -0.6	5.9 1.9	0.503 0.529	0.781 0.848	0.213 0.148	0.110	0.040	0.021
4	40.40	2.7	-1.6	3.8	0.554	0.830	0.163	0.096	0.032	0.019
5 6	42.80	2.7 2.7	-1.7 -1.8	4.5 5.1	0.562 0.561	0.820 0.827	0.171 0.164	0.106 0.103	0.033 0.031	0.020 0.020
	45.20									
7	47.90	2.7	-2.0	4.7 4.3	0.556	0.855	0.137	0.080	0.026	0.015
7 8 9	47.90 50.00 71.80	2.7 3.0 5.0	-2.0 -1.8 -0.9	4.3 6.0	0.548 0.520	0.874 0.930	0.119 0.071	0.066 0.045	0.023 0.013	0.015 0.013 0.008
7 8	47.90 50.00	2.7 3.0	-2.0 -1.8	4.3	0.548	0.874	0.119	0.066	0.023	0.015 0.013

TABLE IX. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

SHORT BLADE-ANGLE SLOT CASING

(c) Reading number, 763-1651

	RAD	11	ABS	BETAM	REL	BETAM	TOTA	L TEMP	TOTAL	PRESS
RP	IN	OUT	IN	OUT	[N	OUT	IN	RATIO	IN	RAT10
```i	9.622	9.531	0.7	59.3	68.1	55.8	520.2	1.322	14.51	1.996
ż	9.426	9.349	0.8	54.5	66.6	54.0	519.3	1.282	14.66	1.966
-			0.5	51.7	62.3	48.1	519.2	1.242	14.71	1.913
3	8.587	B.607								
4	8.152	8.239	0.3	53.2	59.9	46.2	518.4	1.235	14.72	1.853
5	8.040	8.146	0.3	54.1	59.5	46.0	518.4	1.233	14.72	1.841
6	7.927	8.054	0.1	54.0	56.8	42.6	519.1	1.228	14.72	1.930
7	7.800	7.949	0.2	53.3	58.7	43.4	518.4	1.223	14.72	1.840
8	7.700	7.868	-0.0	52.3	56.0	40.3	518.5	1.219	14.72	1.932
9	6.611	7.025	0.1	51.0	55.4	35.9	517.9	1.186	14.72	1.725
10	5.681	6.387	0.2	50.6	53.5	25.5	518.2	1.176	14.72	1.713
11	5.377	6.201	-0.1	51.2	53.2	20.0	518.4	1.182	14,71	1.742
	ABS	VEL	REL	VEL	MERI	D VEL	TAN	G VEL	WHEEL	SPEED
RP	IN	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT
1	538.9	826.4	1442.0	750.3	538.8	421.9	6.3	710.6	1343.8	1331.1
ż	566.8	810.4	1427.1	799.5	566.7	470.2	7.7	660.1	1317.4	
3	627.8	815.3	1349.3	756.8	627.8	505.5	5.5	639.6	1199.9	
4	657.9	806.9	1312.0	699.5	657.9	483.8	3.7	645.7	1138.8	
-			1302.7	679.9	661.3	472.4	3.7	651.9	1126.1	
5 6	661.3	805.1								
5	726.1	834.9	1324.7	666.2	726.1	490.3	1.2	675.8	1109.1	
7	663.1	814.2	1275.7	670.0	663.1	486.8	2.2	652.6	1092.0	
8	728.4	841.2	1301.2	673.7	728.4	514.0	-0.3	665.9	1078.0	
9	636.1	796.5	1120.8	619.3	636.1	501.6	1.3	618.7	924.1	982.0
10	586.1	829.9	985.5	583.3	586.1	526.4	1.9	641.7	794.2	892.9
11	564.0	862.0	941.0	574.5	564.0	540.0	-0.6	671.9	752.6	867.9
RP	ABS M	ACH NO OUT	REL M	ACH NO OUT	MERID M	ACH NO OUT				PEAK SS MACH NO
1	0.494	0.671	1,321	0.609	0.494	0.343				1.696
2	0.521		1,312	0.660					u./85	
3		0.669	1.312	U. DOU	0.521	0.388			0.783 0.830	
		0.669 0.685			0.521 0.581	0.388			0.830	1.682
ă	0.581	0.685	1.248	0.636	0.581	0.425			0.830 0.805	1.682 1.641
4	0.581	0.685 0.680	1.248	0.636 0.589	0.581 0.611	0.425 0.408			0.830 0.805 0.735	1.682 1.641 1.585
4	0.581 0.611 0.615	0.685 0.680 0.679	1.248 1.219 1.211	0.636 0.589 0.573	0.581 0.611 0.615	0.425 0.408 0.398			0.830 0.805 0.735 0.714	1.682 1.641 1.585 1.579
4 5 6	0.581 0.611 0.615 0.680	0.685 0.680 0.679 0.708	1.248 1.219 1.211 1.240	0.636 0.589 0.573 0.565	0.581 0.611 0.615 0.680	0.425 0.408 0.398 0.415			0.830 0.805 0.735 0.714 0.675	1.682 1.641 1.585 1.579 1.528
4 5 6 7	0.581 0.611 0.615 0.680 0.616	0.685 0.680 0.679 0.708 0.690	1.248 1.219 1.211 1.240 1.186	0.636 0.589 0.573 0.565 0.568	0.581 0.611 0.615 0.680 0.616	0.425 0.408 0.398 0.415 0.413			0.830 0.805 0.735 0.714 0.675 0.734	1.641 1.585 1.579 1.528 1.563
4 5 6 7 8	0.581 0.611 0.615 0.680 0.616 0.682	0.685 0.680 0.679 0.708 0.690 0.717	1.248 1.219 1.211 1.240 1.186 1.219	0.636 0.589 0.573 0.565 0.568 0.574	0.581 0.611 0.615 0.680 0.616 0.682	0.425 0.408 0.398 0.415 0.413 0.438			0.830 0.805 0.735 0.714 0.675 0.734 0.706	1.682 1.641 1.585 1.579 1.528 1.563 1.512
4 5 6 7 8 9	0.581 0.611 0.615 0.680 0.616 0.682 0.590	0.685 0.680 0.679 0.708 0.690 0.717 0.686	1.248 1.219 1.211 1.240 1.186 1.219 1.039	0.636 0.589 0.573 0.565 0.568 0.574 0.533	0.581 0.611 0.615 0.680 0.616 0.682 0.590	0.425 0.408 0.398 0.415 0.413 0.438 0.432			0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789	1.682 1.641 1.585 1.579 1.528 1.563 1.512
4 5 6 7 8 9	0.581 0.615 0.680 0.616 0.682 0.590 0.540	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457			0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898	1.682 1.641 1.585 1.579 1.528 1.563 1.512 1.502 1.298
4 5 6 7 8 9	0.581 0.611 0.615 0.680 0.616 0.682 0.590	0.685 0.680 0.679 0.708 0.690 0.717 0.686	1.248 1.219 1.211 1.240 1.186 1.219 1.039	0.636 0.589 0.573 0.565 0.568 0.574 0.533	0.581 0.611 0.615 0.680 0.616 0.682 0.590	0.425 0.408 0.398 0.415 0.413 0.438 0.432			0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789	1.682 1.641 1.585 1.579 1.528 1.563 1.512
4 5 6 7 8 9	0.581 0.615 0.680 0.616 0.682 0.590 0.540	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457			0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898	1.682 1.641 1.585 1.579 1.528 1.563 1.512 1.502 1.298
4 5 6 7 8 9	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909 0.866	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469	1055 (	OEFF	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957	1.682 1.641 1.585 1.579 1.528 1.563 1.512 1.502 1.298 1.244
4 5 6 7 8 9 10	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909 0.866	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469	LOSS C		0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957	1.682 1.641 1.585 1.579 1.528 1.563 1.512 1.502 1.298 1.244
4 5 6 7 8 9 10 11	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909 0.866	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469	TOT	PR0F	0.830 0.805 0.735 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957	1.682 1.641 1.585 1.579 1.528 1.563 1.512 1.502 1.298 1.244 ARAM PROF
4 5 6 7 8 9 10 11	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909 0.866 IDENCE SS 4.3	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499 DEV	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469 EFF	TOT 0.378	PROF 0.266	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.957 LOSS P	1.682 1.641 1.589 1.579 1.528 1.563 1.512 1.502 1.298 1.244 ARAM PROF 0.049
4 5 6 7 8 9 10 11	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6	1.248 1.219 1.211 1.240 1.186 1.219 1.039 0.909 0.866 IDENCE SS 4.3 3.5	0.636 0.589 0.573 0.565 0.564 0.574 0.533 0.506 0.499 DEV 7.0 5.8	0.581 0.611 0.681 0.680 0.616 0.682 0.590 0.540 0.519 D-FACT 0.638 0.586	0.425 0.408 0.398 0.415 0.415 0.432 0.457 0.469 EFF 0.677 0.757	TOT 0.378 0.268	PROF 0.266 0.160	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957	1.682 1.641 1.589 1.579 1.528 1.563 1.512 1.502 1.298 1.244 ARAM PROF 0.049
4 5 6 7 8 9 10 11	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70 30.90	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866 IDENCE SS 4,3 3,5 2,2	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499 DEV 7.0 5.8 3.1	0.581 0.611 0.615 0.680 0.616 0.692 0.590 0.540 0.519 D-FACT	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469 EFF 0.677 0.757	TOT 0.378 0.268 0.171	PROF 0.266 0.160 0.083	0.830 0.805 0.735 0.714 0.675 0.734 0.769 0.898 0.957 LOSS P TOT 0.070 0.050 0.033	1.682 1.641 1.587 1.579 1.528 1.563 1.512 1.502 1.244 ARAM PROF 0.049 0.030 0.016
4 5 6 7 8 9 10 11 RP 1 2 3	0.581 0.611 0.615 0.680 0.616 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.6	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866 IDENCE SS 4,3 3,5 2,2 1,3	0.636 0.589 0.573 0.565 0.568 0.574 0.536 0.499 DEV 7.0 5.8 3.1 3.9	0.581 0.615 0.605 0.680 0.616 0.582 0.590 0.519 D-FACT 0.638 0.586 0.587 0.604	0.425 0.408 0.398 0.415 0.413 0.438 0.457 0.469 EFF 0.677 0.757 0.841 0.819	TOT 0.378 0.268 0.171 0.196	PROF 0.266 0.160 0.083 0.125	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957 LOSS P TOT 0.070 0.053 0.033	1.682 1.641 1.589 1.579 1.528 1.563 1.512 1.502 1.298 1.244 ARAM PROF 0.049 0.030 0.016
4 5 6 7 8 9 10 11 RP 1 2 3	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80	0.685 0.680 0.6708 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.6	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866 IDENCE SS 4,3 3,5 2,2 1,3	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.505 0.499 DEV 7.0 5.8 3.1 3.9	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 D-FACT 0.638 0.586 0.576 0.604	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469 EFF 0.677 0.757 0.819 0.817	TOT 0.378 0.268 0.171 0.196 0.198	PROF 0.266 0.160 0.083 0.125 0.130	0.830 0.805 0.735 0.734 0.675 0.734 0.706 0.789 0.898 0.957 LOSS P TOT 0.070 0.053 0.038	1.682 1.641 1.579 1.528 1.563 1.512 1.502 1.244 ARAM PROF 0.049 0.030 0.016
4567891011 RP123456	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20	0.685 0.680 0.6708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.6 5.8	1,248 1,219 1,211 1,240 1,186 1,219 1,039 0,909 0,866 IDENCE SS 4,3 3,5 2,2 1,3 -1,0	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499 DEV 7.0 5.8 3.1 3.9 4.5	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 D-FACT 0.638 0.586 0.577 0.604 0.637	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469 EFF 0.677 0.757 0.841 0.819 0.905	TOT 0.378 0.268 0.171 0.196 0.198 0.101	PROF 0.266 0.160 0.083 0.125 0.130 0.039	0.830 0.805 0.735 0.714 0.675 0.736 0.789 0.898 0.957 LOSS P TOT 0.070 0.050 0.038 0.038	1.682 1.641 1.587 1.579 1.528 1.5612 1.502 1.298 1.244 ARAM PROF 0.049 0.030 0.016 0.025 0.025
4 5 6 7 8 9 10 11 RP 1 2 3 4 5 6 7	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 47.90	0.685 0.689 0.708 0.690 0.717 0.696 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.6 5.8 3.5 6.0	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866 IDENCE SS 4,3 3,5 2,2 1,3 1,3 -1,0	0.636 0.589 0.573 0.565 0.568 0.574 0.536 0.499 DEV 7.0 5.8 3.1 3.9 4.5 1.9	0.581 0.615 0.680 0.616 0.592 0.590 0.540 0.519 D-FACT 0.638 0.577 0.604 0.637 0.616	0.425 0.408 0.398 0.415 0.413 0.438 0.457 0.469 EFF 0.677 0.757 0.841 0.819 0.817 0.954	TOT 0.378 0.268 0.171 0.196 0.198 0.101 0.158	PROF 0.266 0.160 0.083 0.125 0.130 0.039 0.097	0.830 0.805 0.735 0.714 0.675 0.734 0.789 0.898 0.957 LOSS P TOT 0.050 0.033 0.038 0.038	1.682 1.641 1.5879 1.579 1.528 1.563 1.512 1.502 1.298 1.244 ARAM PROF 0.049 0.030 0.016 0.024 0.024 0.028 0.019
456789111 RP 12345678	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 47.90 50.00	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.8 3.5 6.8	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866 IDENCE SS 4,3 3,5 2,2 1,3 1,3 -1,0 1,4	0.636 0.589 0.573 0.565 0.568 0.574 0.536 0.506 0.499 DEV 7.0 5.8 3.1 3.9 4.5 1.9	0.581 0.615 0.680 0.616 0.692 0.590 0.519 D-FACT 0.638 0.586 0.577 0.604 0.616 0.637 0.613	0.425 0.408 0.398 0.415 0.413 0.438 0.457 0.469 EFF 0.677 0.757 0.819 0.817 0.944	TOT 0.378 0.268 0.171 0.196 0.198 0.101 0.158 0.059	PROF 0.266 0.160 0.083 0.125 0.130 0.039 0.097 0.003	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957 LOSS P TOT 0.070 0.053 0.038 0.038 0.031 0.012	1.682 1.641 1.579 1.579 1.528 1.563 1.512 1.502 1.244 ARAM PROF 0.049 0.030 0.016 0.024 0.025 0.001
456789111 RP 1233456789	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 PERCENT SPAN 7.00 11.70 30.90 42.80 45.20 47.90 50.00 71.80	0.685 0.680 0.6708 0.708 0.707 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.8 3.5 6.0	1,248 1,219 1,211 1,240 1,186 1,219 0,909 0,866  IDENCE SS 4,3 3,5 2,2 1,3 -1,0 1,4 -1,0 1,9	0.636 0.589 0.573 0.565 0.568 0.574 0.533 0.506 0.499 DEV 7.0 5.8 3.1 4.5 1.9 3.7 6.8	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.540 0.519 D-FACT 0.638 0.596 0.577 0.613 0.613 0.613	0.425 0.408 0.398 0.415 0.413 0.438 0.432 0.457 0.469 EFF 0.677 0.757 0.841 0.905 0.817 0.905 0.905	TOT 0.378 0.268 0.171 0.196 0.198 0.101 0.158 0.059 0.105	PROF 0.266 0.160 0.083 0.125 0.130 0.039 0.097 0.003	0.830 0.805 0.735 0.734 0.675 0.734 0.706 0.789 0.957 LOSS P TOT 0.070 0.053 0.033 0.038 0.038 0.031 0.012	1.682 1.641 1.579 1.528 1.563 1.512 1.502 1.244 ARAM PROF 0.049 0.030 0.016 0.024 0.025 0.008
456789111 RP 12345678	0.581 0.611 0.615 0.680 0.616 0.682 0.590 0.519 PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 47.90 50.00	0.685 0.680 0.679 0.708 0.690 0.717 0.686 0.720 0.749 INC MEAN 6.6 6.1 6.0 5.8 3.5 6.8	1,248 1,219 1,211 1,240 1,186 1,219 1,039 0,909 0,866  IDENCE SS 4,3 3,5 2,2 1,3 -1,0 1,4 -1,0 1,9	0.636 0.589 0.573 0.565 0.568 0.574 0.536 0.506 0.499 DEV 7.0 5.8 3.1 3.9 4.5 1.9	0.581 0.615 0.680 0.616 0.692 0.590 0.519 D-FACT 0.638 0.586 0.577 0.604 0.616 0.637 0.613	0.425 0.408 0.398 0.415 0.413 0.438 0.457 0.469 EFF 0.677 0.757 0.819 0.817 0.944	TOT 0.378 0.268 0.171 0.196 0.198 0.101 0.158 0.059	PROF 0.266 0.160 0.083 0.125 0.130 0.039 0.097 0.003	0.830 0.805 0.735 0.714 0.675 0.734 0.706 0.789 0.898 0.957 LOSS P TOT 0.070 0.053 0.038 0.038 0.031 0.012	1.682 1.641 1.579 1.579 1.528 1.563 1.512 1.502 1.244 ARAM PROF 0.049 0.030 0.016 0.024 0.025 0.001

TABLE IX. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES FOR SHALLOW,

#### SHORT BLADE-ANGLE SLOT CASING

## (d) Reading number, 764-1662

RP 1 2 3 4 5 6 7 8 9 10	RAI IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 0.9 0.7 0.2 0.1 0.1 -0.2 -0.0 0.1	BETAM OUT 65.0 60.2 54.9 55.8 56.2 55.6 54.9 53.8 51.8 52.5	RELIN 70.4 68.9 62.7 60.7 61.8 61.5 58.9 55.3	BETAM OUT 56.8 54.5 48.4 46.2 43.6 44.6 43.3 42.6 35.9 25.6 19.8	TOTA IN 520.1 519.8 519.8 518.7 519.0 518.6 517.9 518.0 517.8	AL TEMP RAT 10 1.357 1.310 1.252 1.246 1.241 1.238 1.234 1.227 1.194 1.180	TOTAL IN 14.51 14.65 14.72 14.72 14.72 14.72 14.72 14.72 14.72	PRESS RAT10 2.054 2.013 1.940 1.888 1.958 1.868 1.869 1.741 1.733 1.753
RP 1 2 3 4 5 6 7 8 9	ABS IN 477.7 505.5 561.6 587.0 629.5 592.9 592.4 591.0 578.8 537.0 518.8	WEL 0UT 858.6 836.6 820.6 815.1 835.3 816.6 819.6 816.8 795.4 826.3 855.9	RELL IN 1420.7 1404.1 1318.9 1280.5 1285.4 1255.5 1241.1 1230.2 1090.8 958.7 911.7	VEL OUT 663.5 714.7 710.8 662.4 642.5 637.2 635.7 638.3 579.6 567.0 553.5	MERI IN 477.7 505.4 561.5 587.0 629.5 592.4 591.0 578.8 537.0 518.8	D VEL OUT 363.5 415.5 471.7 458.1 465.2 453.8 462.6 469.5 469.4 511.4 520.9	TAN IN 7.7 8.4 7.1 2.5 1.4 1.1 1.1 -1.7 -0.2 1.1	6 VEL 0UT 777.9 726.1 671.5 674.2 693.8 678.5 668.4 642.1 649.1 679.2	HHEEL IN 1345.6 1318.3 1200.5 1140.5 1122.1 1107.8 1091.7 1077.2 924.3 795.3 751.2	1307.6 1203.3 1152.7 1136.9 1125.6 1112.6 1100.7 982.2 894.1
RP 1 2 3 4 5 6 7 8 9 10	ABS M IN 0.435 0.462 0.516 0.583 0.547 0.547 0.545 0.543 0.475	ACH NO OUT 0.690 0.684 0.687 0.684 0.704 0.687 0.682 0.692 0.692 0.692 0.716 0.743	REL M/ IN 1.295 1.283 1.212 1.180 1.190 1.158 1.145 1.135 1.005 0.880 0.835	OUT 0.533 0.584 0.595 0.556 0.541 0.537 0.537 0.541 0.497 0.491 0.480	MERID M/ IN 0.435 0.462 0.516 0.541 0.547 0.547 0.545 0.533 0.493	ACH NO OUT 0.292 0.340 0.395 0.384 0.392 0.382 0.391 0.391 0.403 0.443			MERID I VEL R I 0.761 0.822 0.840 0.780 0.739 0.765 0.781 0.794 0.811 0.952	PEAK SS MACH NO 1.749 1.733 1.694 1.602 1.631 1.627 1.625 1.577 1.332 1.263
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 8.9 8.5 8.4 6.9 8.6 8.9 9.1 10.3	DENCE SS 6.6 5.8 4.7 4.2 2.5 4.1 4.2 4.3 4.4 4.7	DEV 8.0 6.2 3.4 3.9 2.1 3.6 3.7 6.8 6.5 4.2	D-FACT 0.709 0.654 0.609 0.630 0.650 0.641 0.635 0.627 0.607 0.547	0.640 0.714 0.826 0.810 0.876 0.821 0.836 0.854 0.884 0.948	LOSS CO TOT 0.455 0.340 0.199 0.220 0.143 0.209 0.192 0.170 0.143 0.076 0.088	DEFF PROF 0.333 0.225 0.104 0.141 0.073 0.137 0.123 0.103 0.103 0.073	LOSS PATOT 0.081 0.063 0.039 0.043 0.028 0.043 0.037 0.033 0.026 0.013 0.015	ARAM PROF 0.060 0.042 0.020 0.027 0.014 0.027 0.024 0.020 0.019 0.013

TABLE X. - BLADE-ELEMENT DATA AT BLADE EDGES FOR SKEWED SLOT CASING

			•	•	-	•				
	RAD			BETAM		BETAM		L TEMP		. PRESS
RP	[N	OUT	IN	OUT	IN	OUT	IN	RATIO	IN	RATIO
1	9.622	9.531	2.3	53.5	69.9	55.5	519.9	1.357	14.55	2.040 2.101
2 3	9.426	9.349	2.9	54.5	68.7	50.4 51.7	519.0 524.8	1.369	14.67	1.912
4	8.587	8.607	3.0 1.6	53.4 58.0	64.6 61.8	49.1	517.4	1.247	14.73	1.890
•	8.152 8.040	8.239 8.146	1.5	58.6	61.3	48.7	517.5	1.243	14.73	1.871
5	7.927	8.054	1.5	58.4	61.1	47.8	517.0	1.241	14.73	1.866
7	7.800	7.949	1.6	58.0	60.7	46.5	517.4	1.236	14.73	1.861
8	7.700	7.868	1.6	57.3	60.4	45.8	517.0	1.231	14.73	1.850
9	6.611	7.025	1.1	55.9	58.2	37.0	516.6	1,203	14.73	1.762
10	5.681	6.387	1.3	52.6	54.9	25.1	517.2	1.180	14.73	1,805
11	5.377	6.201	1.5	53.6	56.0	20.6	516.9	1.191	14.72	1.768
							<b>7.</b>			COULD
••		VEL		VEL		D VEL		G VEL		SPEED
RP	IN	OUT	IN.	0UT	[N	0UT	IN 10 F	OUT	[N	0UT 1335.6
1	485.7	800.0	1414.8	839.7	485.3	475.4	19.5	643.5 702.0		1307.2
2	505.1	862.2 775.5	1387.2 1300.6	785.3 745.8	504.5 557.4	500.5 462.5	25.7 29.5	622.4		1207.4
3 4	558.2 603.0	790.5	1276.4	640.3	602.7	419.2	16.9	670.2		1154.2
Ē	606.0	787.4	1262.0	623.0	605.8	410.8	18.3	671.7		1140.2
5	605.0	789.4	1249.9	615.0	604.8	413.3	16.3	672.5		1127.9
7	603.6	791.9	1233.3	608.4	603.4	419.1	16.4	671.9		1112.9
8	602.6	788.7	1219.8	611.1	602.3	426.3	17.2	663.6		1101.5
9	568.8	787.6	1078.3	553.4	568.7	442.1	10.4	651.8	926.6	984.6
10	549.6	828.7	956.6	556.2	549.5	503.5	12.6	658.1	795.6	894.5
11	499.8	844.6	893.3	535.0	499.7	500.7	12.7	680.2	753.2	868.7
	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO			MERID	PEAK SS
RP	IN	OUT	[N	OUT	IN	0UT				MACH NO
1	0.443	0.639	1.290	0.671	0.443	0.380			0.979	1,731
2	0.462	0.691	1.269	0.629	0.461	0.401			0.992	1.713
3	0.510	0.645	1.188	0.621	0.509	0.385			0.830	1.669
4	0.557	0.662	1.180	0.536	0.557	0.351			0.696	1.618
5 6	0.560	0.660	1.167	0.523 0.517	0.560 0.559	0.345 0.347			0.678 0.683	1.605 1.604
7	0.560 0.558	0.663 0.667	1.156 1.140	0.512	0.558	0.353			0.695	1.597
é	0.557	0.665	1.128	0.515	0.557	0.360			0.708	1.591
9	0.524	0.673	0.994	0.473	0.524	0.378			0.777	
10	0.505	0.719	0.880	0.482	0.505	0.437			0.916	1.301
11	0.458	0.730	0.818	0.463	0,458	0.433			1.002	
• • •		••••			-,					
					B =:			٥٣٣٣	1.000	DADAM
20	PERCENT		IDENCE	DEV	D-FACT	EFF	LOSS C	OEFF PROF	LOSS 1	PARAM
RP	SPAN	MEAN		c 7	A FEA	A C#3	TOT			0.065
1	7.00	8.4		6.7	0.550	0.632	0.466 0.476	0.349	0.086 0.097	
2 3 4	11.70 30.90	8.1 8.3	5.6 4.5	2.2 6.7	0.589 0.561	0.640 0.845	u.476	0.090	0.032	
3	40.40	7,6		6.8	0.642	0.806	0.225	0.153	0.041	0.028
5	42.80	7.6		7.2	0.650	0.806	0.226	0.159	0.041	0.029
ř	45.20	7.8		7, 1	0.652	0.810	0.223	0.157	0.041	0.029
6 7	47.90	8.1	3.4	6.7	0.651	0.824	0.207	0.146	0.038	
8	50.00	8.2		6.8	0.641	0.831	0.200	0.141	0.037	
9	71.80	10.5	4.6	7.8	0.626	0.866	0.173	0.147	0.031	0.027
10	88.30	10.2		6.1	0.557	1.018	-0.027			-0.005
11	93.10	12.0	5.3	5.1	0.547	0.924	0.130	0.130	0.022	0.022

TABLE X. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR  $\tt KEWED$  SLOT CASING

#### (b) Reading number, 510-940

			(r	) Readii	ng numo	er, sio	-940			
RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	9.531 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.3 1.5 2.2 1.4 1.3 1.3 1.4 1.3	BETAM OUT 49.2 48.2 47.0 49.4 49.4 48.5 47.8 46.2 46.7 48.4	RELL IN 67.5 66.3 60.5 57.6 56.8 56.4 56.0 55.6 53.8 51.2	BETAM OUT 56.5 52.2 47.4 48.9 48.1 46.5 45.4 28.4 21.9	TOTA IN 520.8 519.7 519.1 518.3 518.0 518.6 518.1 518.2 518.2	RATIO 1.340 1.347 1.231 1.215 1.211 1.202 1.202 1.179 1.170 1.183	TOTAL IN 14.51 14.68 14.71 14.73 14.74 14.74 14.74 14.74 14.74 14.74	PRESS RATIO 1.872 1.921 1.896 1.772 1.743 1.737 1.741 1.748 1.704 1.669 1.706
RP 1 2 3 4 5 6 7 8 9 10 11	ABS IN 554.5 576.0 670.4 718.3 728.7 729.9 730.2 684.5 616.4 595.0	VEL 0UT 767.7 818.7 817.3 772.3 761.3 763.2 772.7 778.8 802.6 818.6 861.5	REL IN 1450.9 1430.6 1360.2 1338.4 1331.6 1391.8 1304.7 1291.8 1142.3 996.7 950.2	VEL 0UT 909.9 890.6 830.0 767.1 753.8 745.0 744.8 745.0 690.0 638.3 616.9	MERI 1N 554.4 669.9 718.1 728.5 729.7 730.0 684.3 616.2 594.8	D VEL 0UT 501.6 545.8 557.8 506.4 495.4 497.1 512.5 523.5 555.6 561.6 572.5	TAN IN 12.4 15.1 25.4 17.5 16.3 17.3 15.5 16.0	G VEL 0UT 581.2 597.4 583.0 578.0 579.1 579.1 579.5 579.5 643.8	IN 1353.2	1159.2 1146.1 1133.9 1118.8
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.508 0.530 0.623 0.672 0.684 0.684 0.684 0.638 0.570 0.549	ACH NO OUT 0.615 0.658 0.690 0.654 0.645 0.645 0.658 0.669 0.712	REL M IN 1.330 1.316 1.264 1.253 1.248 1.237 1.222 1.211 1.065 0.922 0.877	ACH NO OUT 0.729 0.716 0.701 0.650 0.639 0.633 0.634 0.636 0.556 0.555	MERID M IN 0.508 0.530 0.623 0.672 0.683 0.684 0.684 0.684 0.638 0.579	ACH NO OUT 0.402 0.439 0.471 0.429 0.420 0.422 0.436 0.447 0.480 0.488 0.497				PEAK SS MACH NO 1.687 1.675 1.595 1.536 1.522 1.514 1.503 1.493 1.439 1.263
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 6.0 5.7 4.2 3.3 3.1 3.2 3.3 5.5 7.1	SS 3.7 3.1 0.4 -1.0 -1.3 -1.3 -1.4 -0.4 0.5 0.6	7.7 4.0 2.8 6.4 7.4 7.5 6.8 7.2 9.3 6.3	D-FACT 0.500 0.510 0.513 0.546 0.551 0.553 0.546 0.539 0.512 0.479 0.480	EFF 0.577 0.591 0.867 0.827 0.817 0.824 0.849 0.866 0.918 0.926 0.899	LOSS C TOT 0.494 0.493 0.137 0.169 0.178 0.171 0.147 0.131 0.089 0.096 0.150	OEFF PROF 0.383 0.387 0.058 0.104 0.116 0.112 0.092 0.079 0.063 0.094 0.150	LOSS F TOT 0.089 0.097 0.027 0.031 0.032 0.031 0.027 0.024 0.016 0.016	PROF 0.069 0.076 0.011 0.019 0.021 0.020 0.017 0.015 0.012 0.016 0.025

TABLE X. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR SKEWED

#### SLOT CASING

## (c) Reading number, 511-951

			400	DET	<b>6</b> C.	DETIN	707*	I TEMP	TAT 21	00555
RP	RAD IN	OUT	IN AB2	BETAM OUT	IN	BETAM OUT	IN	RATIO	IN	PRESS RATIO
1	9.622	9.531	1,4	52.0	69.2	54.4	521.0	1.363	14.52	2.059
2	9.426	9.349	1.5	52.0	68.0	49.8	519.5	1.369	14.60	2.109
2 3 4	8.587	8.607	2.3	52.0	63.0	48.7	519.4	1.250	14.68	1.978
5	8.152 8.040	8.239 8.146	1.5 1.5	55.2 55.9	60.3 59.8	48.8 48.3	518.4 517.9	1.242	14.72 14.72	1.880
6	7.927	8.054	1.4	55.5	59.8	48.3	518.4	1.233	14.74	1.860
7	7.800	7.949	1.6	54.7	59.1	46.0	518.5	1.228	14.73	1.857
8	7.700	7.868	1.4	54.1	58.8	45.1	518.2	1.225	14.74	1.854
9	6.611	7.025	1.4	52.7	56.2	37.3	517.7	1.196	14.74	1.756
10	5.681	6.387	1.4	51.5	54.8	27.9	518.3	1.181	14.73	1.727
11	5.377	6.201	1.5	52.6	54.3	20.9	518.3	1.192	14.74	1.762
			DE		MED!	S	7.55	c	. 11. 1551	COEED
RP	IN	VEL OUT	REL IN	OUT	MERI [N	D VEL OUT	I AN	G VEL OUT	IN	SPEED
1	509.1	813.9	1435.2	861.4	509.0	501.4	12.5	641.2	1354.5	
2	529.6	866.2	1413.4	825.2	529.4	532.7	13.5	683.0	1324.1	
3	603.0	812.4	1327.9	757.9	602.5	499.7	24.2	640.6	1207.5	
4	645.0	786.3	1301.0	682.5	644.8	449.2	17.0	645.4	1147.0	
5 6	648.7 653.0	785.0 787.0	1287.8 1277.9	662.8 657.4	648.5 652.8	440.6 445.2	17.4 16.3	649.7 649.0	1130.0 1114.8	
7	647.9	791.8	1259.9	658.1	647.7	457.5	17.7	646.3	1098.4	
8	648.0	792.4	1249.5	658.4	647.8	464.6	16.3	641.9	1084.8	
9	613.8	785.8	1101.7	598.2	613.6	475.8	14.9	625.5	929.9	988.1
10	554.5	808.0	961.4	569.2	554.3	503.0	13.8	632.3	799.4	898.7
11	534.7	850.2	915.0	552.7	534.5	516.2	14.2	675.5	756.9	872.9
	ARS M	ACH NO	DEI M	ACH NO	MERID M	ACU NO			MEDIN	DEAK 66
RP	IN	OUT	[N	OUT	IN	OUT				PEAK SS MACH NO
1	0.465	0.649	1.310	0.687	0.465	0.400			0.985	1.726
2	0.485	0.694	1.295	0.661	0.485	0.427			1.006	1.714
3 4	0.556 0.598	0.680 0.659	1.225	0.6 <b>34</b> 0.572	0.556 0.598	0.418			0.829	1.645
5	0.602	0.659	1.196	0.557	0.602	0.370			0.697 0.679	1.588 1.576
ĕ	0.606	0.662	1.186	0.553	0.606	0.375			0.682	1.567
7	0.601	0.668	1.169	0.555	0.601	0.386			0.706	1.563
8	0.601	0.670	1.160	0.557	0.601	0.393			0.717	1.559
9 10	0.568 0.510	0.673 0.698	1,019 0,884	0.512 0.492	0.568 0.509	0.407 0.435			0.775	1.520
11	0.491	0.090	0.839	0.492	0.509	0.446			0.966	1.239
•	••••		*****	•••	••••	••••				
	PERCENT	INC	IDENCE	DEV	D-FACT	EFF	LOSS C	0EFF	LOSS F	ARAM
RP	SPAN	MEAN	SS				TOT	PROF	TOT	PR0F
1	7.00	7.7		5.6	0.542	0.632	0.463	0.345	0.088	0.066
2	11.70	7.5		1.6	0.567	0.644	0.462	0.349	0.095	0.072
3 4	30.90 40.40	6.7 6.0		3.7 6.5	0.566 0.611	0.860 0.818	0.158 0.203	0.073	0.031 0.037	0.014
5	42.80	6.0		6.8	0.622	0.821	0.200	0.135	0.037	0.025
5 6 7	45.20	6.1	1.5	6.7	0.621	0.831	0.189	0.127	0.035	0.023
	47.90	6.4		6.2	0.613	0.848	0.171	0.112	0.032	0.021
B 9	50.00 71.80	6.6		6.2 8.2	0.607 0.587	0.859 0.890	0.159 0.134	0.102	0.030 0.024	0.019
10	88.30	8.5 10.1		8.2 8.8	0.540	0.890	0.134	0.102	0.024	0.018 0.016
11	93.10	10.3		5.4	0.537	0.913	0.144	0.144	0.024	0.024

TABLE X. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES FOR SKEWED

## SLOT CASING

(d) Reading number, 512-962

			(a)	Keaung	g numbe	r, 512-	902			
RP 1 2 3 4 5 6 7 8 9 10	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 2.4 2.5 2.3 1.6 1.6 1.6 1.4 1.1	BETAM OUT 53.9 54.7 53.9 58.7 58.4 57.9 57.3 56.0 52.5 53.6	RELIN 70.6 69.5 64.4 62.3 61.8 61.5 61.2 60.9 58.8 56.3	BETAM 0UT 55.6 50.7 49.1 49.3 48.8 47.7 46.4 45.7 37.1 27.8 20.9	TOTA IN 521.3 520.7 519.4 518.2 518.0 517.7 517.9 517.7 517.8	AL TEMP RAT10 1.359 1.370 1.261 1.249 1.247 1.243 1.238 1.233 1.204	TOTAL IN 14.53 14.59 14.72 14.73 14.73 14.73 14.73 14.73 14.73	PRESS RAT[0 2.051 2.113 1.981 1.896 1.885 1.881 1.870 1.863 1.774
RP 1 22 3 4 5 6 7 8 9 10 11	ABS 169.9 488.8 566.7 592.7 597.0 594.8 595.6 565.6 515.4 498.8	VEL 0UT 802.7 864.5 812.7 791.4 791.9 794.8 795.1 793.7 789.6 805.5 847.0	REL IN 1413.9 1392.9 1312.7 1275.8 1265.3 1251.8 1232.9 1223.7 1079.8 941.6 897.7	VEL 0UT 837.6 787.4 731.0 641.8 625.4 618.6 613.3 613.9 554.3 537.8	MERI 1N 469.5 488.3 596.5 598.2 596.8 594.6 595.5 595.5 595.3 498.7	D VEL 0UT 472.6 499.1 478.6 418.4 412.0 416.4 422.9 428.6 441.9 490.2 502.5	TAN 19.4 21.2 22.4 16.3 176.2 16.4 14.8 10.6 10.9	656.9 677.0 677.0 677.0 676.3 677.0 673.3 668.0 654.3 639.1 681.8	IN 1353.1 1325.7 1206.6 1146.1 1131.9 1116.6 1096.5	1314.9 1209.4 1158.4 1146.8 1134.5
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.428 0.446 0.521 0.547 0.552 0.551 0.549 0.550 0.521 0.472 0.457	ACH NO 0UT 0.640 0.691 0.677 0.662 0.663 0.667 0.669 0.674 0.696 0.731	REL M. 1N 1.286 1.270 1.207 1.177 1.168 1.156 1.138 1.130 0.994 0.863 0.822	ACH NO OUT 0.668 0.629 0.609 0.537 0.524 0.519 0.516 0.517 0.473 0.473	MERID M. IN 0.427 0.445 0.521 0.552 0.551 0.559 0.559 0.521 0.472 0.456	OUT 0.377 0.379 0.399 0.350 0.345 0.345 0.361 0.377 0.423 0.434			MERID   VEL R   1.007   1.022   0.845   0.706   0.689   0.698   0.711   0.720   0.782   0.951   1.008	PEAK SS #ACH NO 1.750 1.741 1.678 1.633 1.622 1.619 1.608 1.502 1.502
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INCI MEAN 9.1 8.9 8.1 8.0 8.3 8.5 10.8 12.1	TDENCE SS 6.8 6.4 4.3 3.8 3.8 3.8 3.9 4.9 5.5 5.6	DEV 6.8 2.4 4.1 7.0 7.3 7.0 6.7 6.8 8.0 8.8 5.3	D-FACT 0.552 0.591 0.585 0.641 0.651 0.647 0.641 0.627 0.548 0.547	EFF 0.635 0.643 0.805 0.806 0.815 0.822 0.834 0.868 0.943 0.917	LOSS CO TOT 0.466 0.473 0.206 0.229 0.229 0.219 0.212 0.197 0.172 0.086 0.143	DEFF PROF 0.345 0.357 0.116 0.157 0.150 0.148 0.134 0.145 0.084 0.142	LOSS P TOT 0.086 0.096 0.040 0.042 0.042 0.040 0.039 0.036 0.031 0.015	ARAM PROF 0.064 0.073 0.022 0.029 0.027 0.027 0.025 0.026 0.014 0.024

TABLE XI. - BLADE-ELEMENT DATA AT BLADE EDGES FOR CIRCUMFERENTIALLY

#### GROOVED CASING

#### (a) Reading number, 602-1227

			(a) Re	ading nu	mber, c	104-1441				
RP 1 2 3 4 5 6 7 8 9 10 11	RAD IN 9.622 9.426 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	0UT 9.531 9.531 9.549 8.607 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.0 1.5 0.9 0.6 0.3 0.3 0.2 0.1	BETAM OUT 61.1 56.0 52.2 53.5 54.4 54.6 53.9 53.0 52.2	REL IN 68.5 67.1 60.6 60.2 59.8 59.4 59.1 55.2 54.5	BETAM OUT 55.9 53.2 47.9 46.4 46.4 45.5 44.2 43.4 36.5 26.7 19.4	TOTA IN 519.8 519.6 518.5 518.5 518.4 518.4 518.4 518.4 518.6	L TEMP RATIO 1.318 1.287 1.247 1.236 1.233 1.231 1.225 1.220 1.189 1.175 1.185	TOTAL IN 14.54 14.65 14.71 14.72 14.72 14.72 14.72 14.72	PRESS RATIO 2.042 2.025 1.947 1.878 1.856 1.850 1.846 1.840 1.735 1.711
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 525.7 550.5 618.1 638.9 641.1 640.6 640.7 605.9 553.3	VEL OUT 837.3 828.2 818.6 805.2 797.6 799.9 803.2 801.8 789.5 815.3 858.5	RELL IN 1434.3 1414.1 1340.5 1299.7 1276.0 1259.8 1248.3 103.8 964.2 917.3	VEL 0UT 721.8 773.6 748.2 694.7 662.2 659.5 663.9 601.1 574.6 553.2	MERI IN 525.7 550.3 618.0 638.6 640.9 641.1 640.6 640.7 605.9 550.3 533.2	D VEL OUT 404.6 463.4 501.4 478.9 464.1 463.8 473.8 473.8 473.1 513.3 521.7	TAN IN 9.0 14.0 9.9 6.4 4.5 3.3 3.0 2.1 1.0	G VEL OUT 733.0 686.5 647.0 647.3 648.7 651.6 649.2 640.6 624.2 633.4 681.8	WHEEL IN 1343.5 1316.6 1199.4 1138.4 1121.4 1106.5 1087.8 1073.5 923.7 793.1 750.8	1305.9 1202.2 1150.5 1136.2 1124.3 1108.6
RP 2 3 4 5 6 7 8 9 10 11	ABS M 1N 0.481 0.505 0.592 0.594 0.594 0.594 0.594 0.566 0.489	ACH NO OUT 0.682 0.683 0.687 0.678 0.675 0.680 0.680 0.680 0.787 0.745	REL M IN 1.313 1.298 1.239 1.205 1.194 1.183 1.168 1.157 1.020 0.886 0.841	ACH NO OUT 0.588 0.638 0.585 0.567 0.559 0.558 0.563 0.516 0.480	MERID M IN 0.481 0.505 0.595 0.594 0.594 0.594 0.594 0.596 0.506 0.489	ACH NO OUT 0.330 0.382 0.421 0.403 0.391 0.391 0.400 0.409 0.415 0.453				PEAK SS MACH NO 1.703 1.686 1.642 1.596 1.588 1.584 1.575 1.569 1.539 1.318 1.247
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 7.0 6.5 6.2 6.3 6.4 6.6 6.9 10.5	4.7 4.0 2.4 2.0 2.1 2.1 2.1 3.2 3.9	7.1 5.0 2.9 4.1 4.9 4.4 4.5 7.3 7.6 3.9	D-FACT 0.661 0.605 0.582 0.604 0.615 0.615 0.605 0.588 0.538	0.711 0.777 0.848 0.835 0.829 0.833 0.849 0.864 0.900 0.950	LOSS C TOT 0.342 0.254 0.167 0.182 0.190 0.185 0.168 0.151 0.119 0.071	OEFF PROF 0.229 0.148 0.081 0.111 0.122 0.120 0.106 0.093 0.084 0.068	LOSS F TOT 0.063 0.049 0.033 0.035 0.035 0.035 0.032 0.029	PARAM PROF 0.042 0.028 0.016 0.021 0.023 0.023 0.023 0.018 0.015 0.012

TABLE XI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR

## CIRCUMFERENTIALLY GROOVED CASING

## (b) Reading number, 603-1238

RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11
PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	ABS M IN 0.564 0.596 0.692 0.734 0.735 0.738 0.739 0.671 0.595 0.572	ABS IN 611.1 643.6 738.1 770.5 778.2 779.6 782.3 783.3 717.5 641.4 618.6	RAI IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681
INC I MEAN 3.9 3.2 1.9 1.4 1.5 1.6 4.5 6.4	ACH NO 0UT 0.655 0.666 0.707 0.657 0.654 0.662 0.672 0.700 0.720 0.758	0UT 786.7 791.8 831.4 787.3 769.9 765.2 773.2 782.3 805.5 823.4 868.5	0UT 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201
DENCE 55 1.6 0.6 -1.9 -2.9 -3.0 -3.1 -3.2 -1.4 -0.4	REL M 1N 1.356 1.348 1.313 1.286 1.275 1.262 1.251 1.095 0.943 0.897	REL IN 1469.1 1454.8 1400.5 1365.2 1365.2 1351.4 1337.6 1325.8 1170.6 1016.8 970.3	ABS IN 0.6 0.9 0.6 0.8 0.4 -0.0 0.4
DEV 6.5 5.0 1.2 4.6 6.1 6.1 5.6 7.0 8.9 5.5	0.729 0.772 0.773 0.675 0.667 0.662 0.662 0.664 0.624 0.575 0.551	VEL 0UT 875.6 918.6 863.6 791.4 781.2 775.2 772.9 773.7 718.4 658.2 631.5	5 BETAM OUT 50.8 45.9 44.0 46.6 46.7 46.6 45.9 45.2 43.9 45.1
D-FACT 0.537 0.491 0.503 0.536 0.539 0.534 0.528 0.498 0.477	MERID M IN 0.564 0.596 0.692 0.726 0.734 0.735 0.738 0.739 0.671 0.595 0.572	MERIN 611.1 643.5 778.2 779.6 782.3 783.3 717.5 641.6	IN 65.4 63.7 58.2
EFF 0.765 0.824 0.879 0.844 0.833 0.834 0.860 0.885 0.944 0.949	ACH NO 0.415 0.463 0.508 0.461 0.450 0.461 0.473 0.504 0.508 0.514	D VEL 0UT 497.6 5507.8 597.8 541.0 527.5 526.2 538.2 551.0 581.3 589.2	BETAM 0UT 55.4 53.2 46.2 46.9 47.3 45.9 44.6 36.1 28.0 21.1
LOSS CO TOT 0.232 0.168 0.116 0.144 0.150 0.125 0.104 0.056 0.060 0.135		TAN IN 6.4 10.4 7.9 10.5 5.0 3.2 4.1 5.3 -0.4 4.1 2.9	TOT/ IN 519.8 519.1 518.6 518.5 518.4 518.4 518.4 518.6 518.7
0EFF PROF 0.127 0.067 0.035 0.080 0.087 0.088 0.069 0.051 0.029 0.057 0.134		G VEL 0UT 609.3 569.1 577.8 572.1 560.7 555.5 555.1 555.4 5583.1 638.1	AL TEMP RAT10 1.253 1.221 1.203 1.198 1.194 1.190 1.187 1.167 1.158
LOSS F TOT 0.043 0.032 0.024 0.027 0.028 0.027 0.023 0.020 0.010 0.010		IN 1342.4 1315.1 1198.2 1137.5 1123.0 1107.0 1089.0	TOTA IN 14.49 14.65 14.72 14.72 14.73 14.72 14.73 14.73
PARAM PROF 0.024 0.013 0.007 0.015 0.016 0.013 0.010 0.005 0.010	PEAK SS MACH NO 1.640 1.620 1.563 1.501 1.498 1.491 1.478 1.466 1.423 1.260	1329.7 1304.4 1201.0 1149.7 1137.8 1124.8 1109.8 1098.5 982.4 891.7 865.5	1.857 1.864 1.741 1.705 1.691 1.698 1.707 1.670

TABLE XI. - Continued. BLADE-ELEMENT DATA AT BLADE EDGES FOR

#### CIRCUMFERENTIALLY GROOVED CASING

## (c) Reading number, 604-1249

RP 1 2 3 4 5 6 7 8 9 10 11	RAD IN 9.622 9.426 8.587 8.152 8.040 7.927 7.800 7.700 6.611 5.681 5.377	011 9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.4 1.2 0.9 0.4 0.3 0.4 0.2 0.1	BETAM 0UT 56.1 52.0 49.7 52.0 52.7 52.5 52.2 51.4 50.1 49.8 51.4	REL IN 66.9 65.5 58.5 58.2 57.7 57.3 57.0 55.6	BETAM 0UT 54.4 52.6 47.2 46.2 46.4 45.9 44.6 43.7 35.8 26.9 19.8	TOTA 1N 519.7 519.3 518.6 518.5 518.8 518.6 518.5 518.4 518.4	IL TEMP RATIO 1.298 1.240 1.230 1.225 1.221 1.216 1.212 1.1184	TOTAL IN 14.52 14.64 14.72 14.72 14.72 14.72 14.72 14.72 14.72	PRESS RAT10 2.026 2.000 1.943 1.863 1.831 1.822 1.820 1.820 1.733
RP 1 2 3 4 5 6 7 8 9 10	ABS IN 568.0 594.2 673.2 693.4 692.0 697.0 695.1 696.0 645.4 583.5 563.1	VEL 0UT 827.0 818.3 822.9 804.7 793.6 791.2 795.5 797.8 797.2 816.8 860.2	REL IN 1445.3 1430.6 1365.9 1328.3 1312.9 1304.1 1287.1 1279.3 1124.2 982.5 933.8	VEL 0UT 792.3 828.6 783.3 715.4 697.4 691.0 685.0 687.9 630.6 591.7 570.2	MERI IN 567.8 594.0 673.1 693.4 692.0 697.0 695.1 696.0 645.4 583.5 563.0	D VEL 0UT 461.5 503.3 532.5 495.5 481.3 481.2 487.7 497.5 511.7 527.7 536.6	TAN 1N 14.0 12.6 10.5 4.9 5.9 5.4 1.8 1.53 5.2	G VEL OUT 686.3 645.2 627.4 634.0 631.0 628.0 628.4 623.6 611.3 623.5 672.4	IN 1343.0 1314.1 1199.0 1137.9 1120.8 1106.1 1088.7	1123.9
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.522 0.548 0.626 0.647 0.645 0.650 0.648 0.649 0.599 0.538 0.518	ACH NO OUT 0.679 0.680 0.693 0.671 0.669 0.675 0.678 0.678 0.678	REL M IN 1,328 1,319 1,271 1,239 1,224 1,216 1,201 1,193 1,043 0,905 0,859	ACH NO 0.651 0.6688 0.660 0.589 0.585 0.581 0.585 0.543 0.495	MERID M 0.522 0.548 0.626 0.647 0.645 0.650 0.648 0.649 0.538 0.518	OUT 0.379 0.418 0.448 0.448 0.407 0.407 0.407 0.404 0.423 0.458 0.466				PEAK SS MACH NO 1.663 1.650 1.556 1.557 1.539 1.537 1.488 1.295 1.227
RP 1 2 3 4 5 6 7 8 9	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 5.4 4.9 4.3 4.4 4.5 4.7 4.8 7.3 8.8	DENCE SS 3.1 2.3 0.4 -0.0 0.0 -0.1 -0.0 0.0 1.4 2.3 2.2	5.6 4.4 2.2 3.9 4.8 5.2 4.9 4.7 6.6 7.8	D-FACT 0.603 0.562 0.559 0.595 0.601 0.602 0.599 0.599 0.566 0.527 0.529	EFF 0.751 0.815 0.870 0.846 0.837 0.846 0.865 0.879 0.925 0.925 0.923	LOSS COTOT 0.281 0.199 0.138 0.161 0.171 0.161 0.127 0.085 0.065 0.118	DEFF PROF 0.176 0.098 0.056 0.094 0.107 0.100 0.084 0.074 0.074	LOSS F TOT 0.053 0.039 0.027 0.031 0.033 0.030 0.027 0.024 0.011 0.020	PROF 0.033 0.019 0.018 0.020 0.019 0.016 0.014 0.011 0.020

TABLE XI. - Concluded. BLADE-ELEMENT DATA AT BLADE EDGES FOR

## CIRCUMFERENTIALLY GROOVED CASING

(d) Reading number, 605-1260

RP 1 2 3 4 5 6 7 8 9 10 11	RAD IN 9.622 9.426 8.587 8.152 8.040 7.700 7.700 6.611 5.681 5.377	9.531 9.349 8.607 8.239 8.146 8.054 7.949 7.868 7.025 6.387 6.201	ABS IN 1.3 1.4 0.9 0.6 0.5 0.3 0.4 0.1	BETAM 0UT 61.0 55.2 51.8 53.3 54.4 54.0 53.3 52.1 50.8 52.4	REL IN 68.3 67.2 62.5 60.4 60.1 59.8 59.3 59.3 54.8	0UT 55.9 53.0 47.9 46.2 46.5 45.5 44.1 43.5 36.3 26.7	TOTA IN 520.0 519.4 518.5 518.7 518.4 518.4 518.4 518.4	RATIO 1.319 1.287 1.245 1.235 1.232 1.229 1.224 1.219 1.188	TOTAL IN 14.56 14.65 14.71 14.71 14.72 14.71 14.72 14.71 14.72	2.014 1.943 1.877 1.849 1.844
RP 1 2 3 4 5 6 7 8 9 10 11	ABS IN 528.5 548.2 617.2 640.0 641.7 642.2 640.7 603.7 548.3 526.9	VEL 0UT 835.5 825.5 816.4 805.5 795.7 983.0 801.4 789.4 815.4 857.8	RELL IN 1431.0 1412.1 1338.4 1296.9 1287.2 1275.1 1257.5 1245.8 1101.0 961.5 913.9	VEL OUT 722.9 784.2 751.8 674.4 663.6 667.6 661.7 576.8 554.9	MERI IN 528.4 548.0 617.2 639.9 641.7 642.2 641.1 640.7 548.3 526.9	D VEL OUT 405.6 471.6 504.4 478.0 464.1 464.8 472.0 479.4 484.9 515.2 523.2	TAN IN 11.6 13.4 9.2 5.1 3.1 5.0 4.8 3.0	G VEL OUT 730.4 677.5 642.0 648.3 648.3 648.7 649.7 649.7 642.1 622.9 632.0 679.8	IN 1341.5 1314.8 1196.7 1134.9 1120.9 1104.7 1086.8	SPEED OUT 1328.8 1304.0 1199.5 1147.0 1135.7 1122.4 1107.6 1096.7 979.2 891.4 864.6
RP 1 2 3 4 5 6 7 8 9 10 11	ABS M IN 0.484 0.503 0.571 0.593 0.595 0.595 0.594 0.558 0.504 0.483	ACH NO OUT 0.680 0.681 0.686 0.679 0.674 0.680 0.678 0.744	REL M IN 1.310 1.296 1.237 1.202 1.193 1.182 1.166 1.155 1.017 0.883 0.838	ACH NO OUT 0.589 0.647 0.582 0.568 0.560 0.557 0.560 0.517 0.500	MERID M IN 0.484 0.503 0.593 0.595 0.595 0.594 0.594 0.558 0.658	ACH NO OUT 0.330 0.389 0.424 0.403 0.391 0.392 0.400 0.407 0.417 0.447				PEAK SS MACH NO 1.695 1.696 1.640 1.589 1.585 1.580 1.570 1.565 1.539 1.315 1.252
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT SPAN 7.00 11.70 30.90 40.40 42.80 45.20 47.90 50.00 71.80 88.30 93.10	INC MEAN 6.8 6.2 6.2 6.4 6.5 6.9 9.1 10.5	IDENCE SS 4.5 4.0 2.4 1.9 1.9 2.0 2.1 3.2 4.0	7.0 4.8 2.8 3.9 5.0 4.9 4.4 4.5 7.2 7.7	D-FACT 0.658 0.595 0.577 0.606 0.614 0.619 0.616 0.607 0.586 0.534 0.537	0.702 0.771 0.854 0.840 0.827 0.836 0.853 0.869 0.907 0.953 0.930	LOSS CO TOT 0.352 0.260 0.160 0.176 0.190 0.182 0.164 0.145 0.111	OEFF PROF 0.242 0.154 0.074 0.107 0.123 0.117 0.104 0.088 0.076 0.064 0.113	LOSS F TOT 0.065 0.050 0.031 0.034 0.036 0.035 0.035 0.028 0.020 0.012	PARAM PROF 0.044 0.030 0.015 0.021 0.023 0.022 0.022 0.020 0.017 0.014 0.011

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